



**QUON HING
CONCRETE CO., LTD.**

Introduction of GGBS concrete

Introduction of Quon Hing

Established in 1985 and registered in Hong Kong as a subsidiary of NWS Holdings.

One of the ready-mix concrete, instant mortar and precast concrete provider to construction and infrastructure industry in Hong Kong.

Concrete

- Two concrete production plants in Tsing Yi and Tai Po
- Annual production capacity more than 750,000m³
- Concrete supplied up to C100
- All GGBS, PFA concrete mixes with Platinum Green Label

MiC

- Operates three industrial parks in GBA, annual production capacity more than 230,000T
- With 25 years of engineering experience in the Guangdong-Hong Kong-Macao
- Specializing in the production of MiC and precast concrete elements



Quon Hing's Green Products

Green and Sustainable Concrete Products

- Negative/Low Carbon Concrete
- Tivoli Green Wall System (Lightweight partition wall)
- H-Crete (Waterproofing Concrete System)
- Smart Drainage Cover (Material for sponge city)
- Capsule Concrete (Lightweight structural concrete)



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1. INTRODUCTION OF GGBS -
 - WHAT IS GGBS?



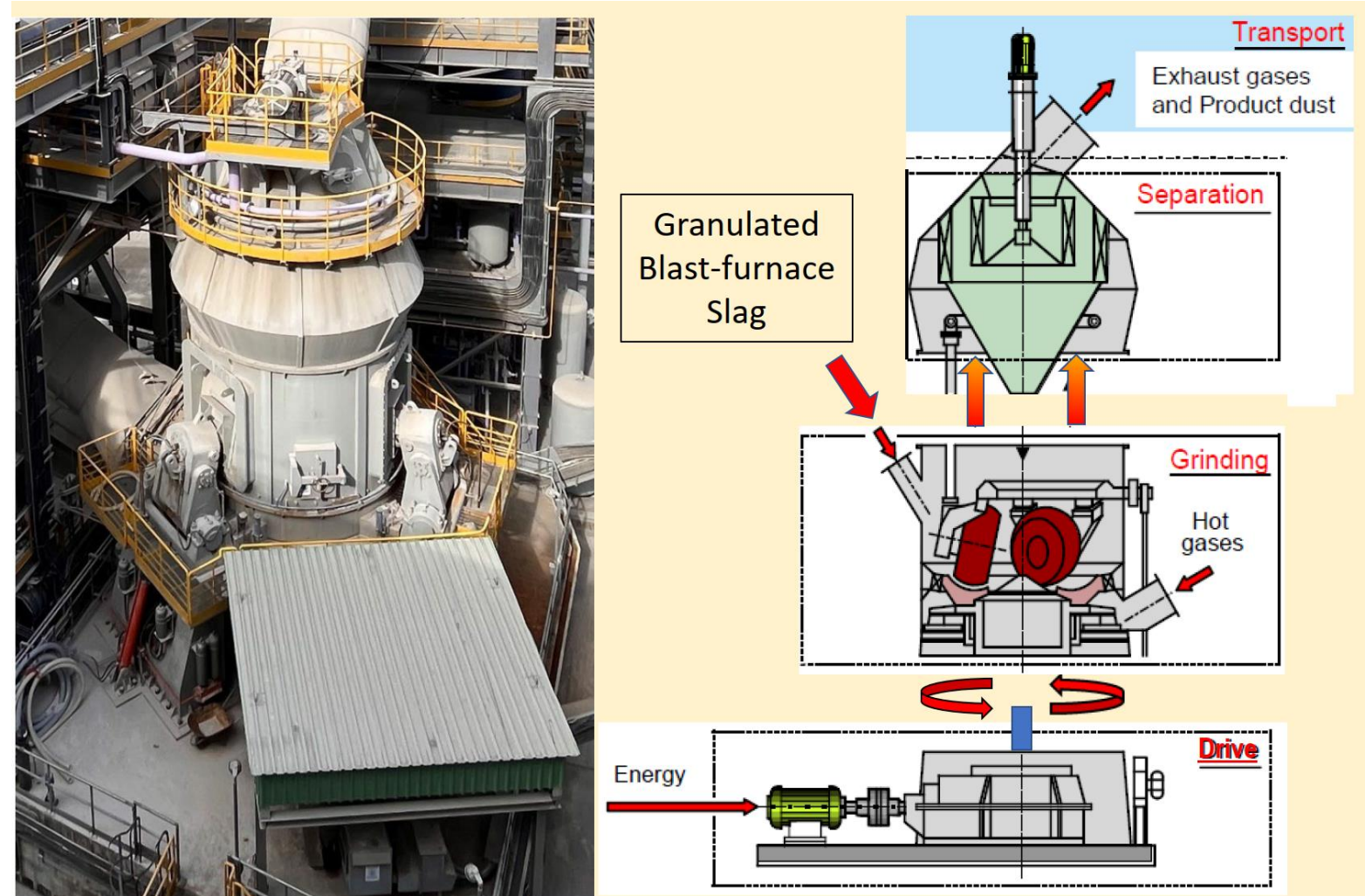
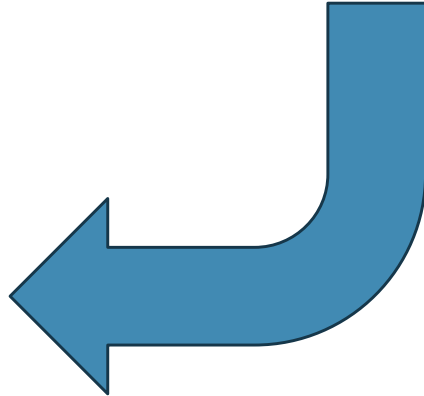
Blast Furnace Slag



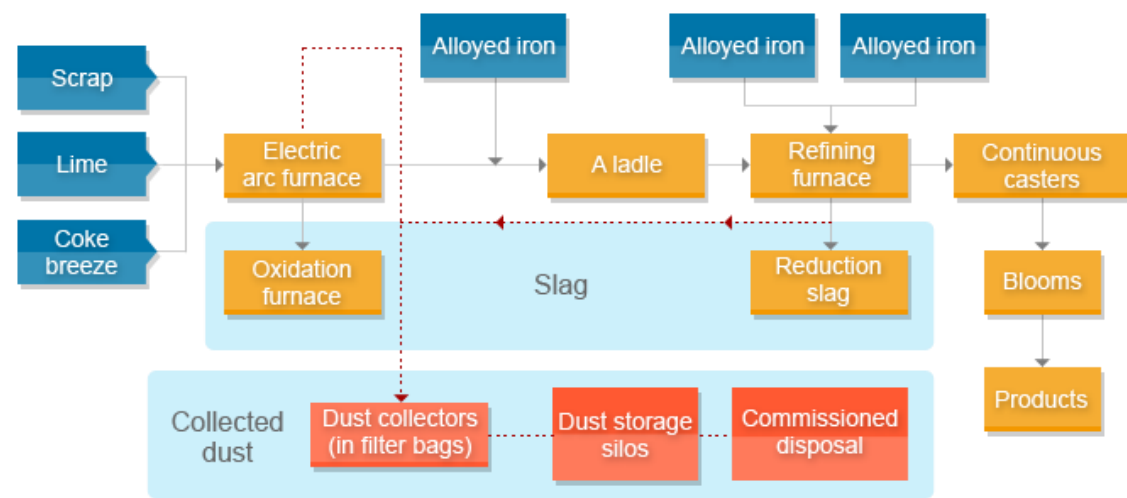
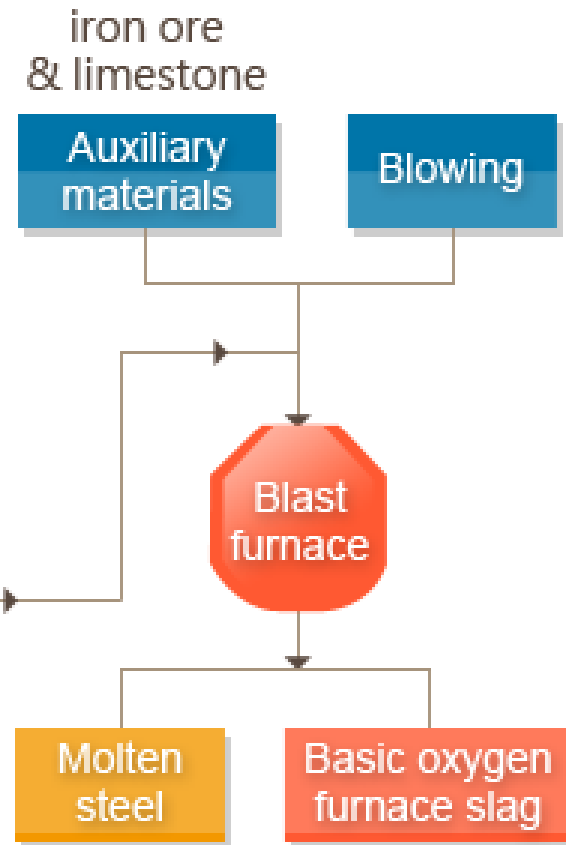
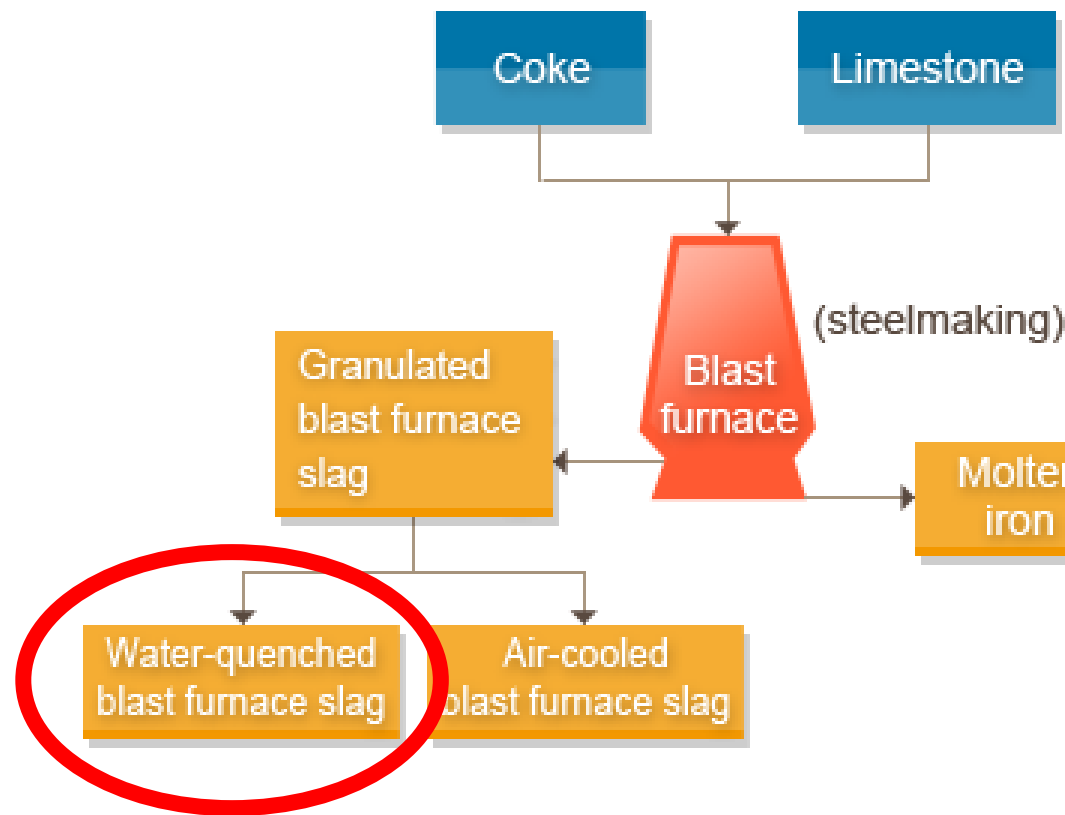
Granulated Blast Furnace Slag



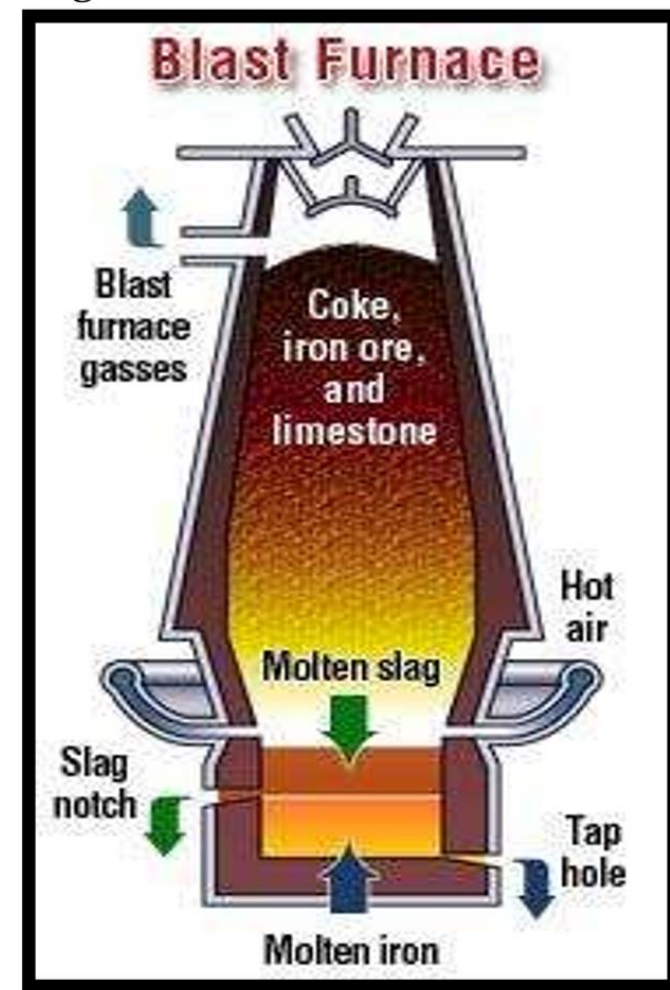
Ground Granulated Blast Furnace Slag



Manufacturing Process



The Production Flow Chart of Slag in an EAF Steel Mill



- **Blast-Furnace Slag (BFS)**

Production process of smelting iron ore, coke, limestone, and other raw materials in a blast furnace is known as blast furnace slag.

- **Basic-Oxygen-Furnace Slag (BOFS)**

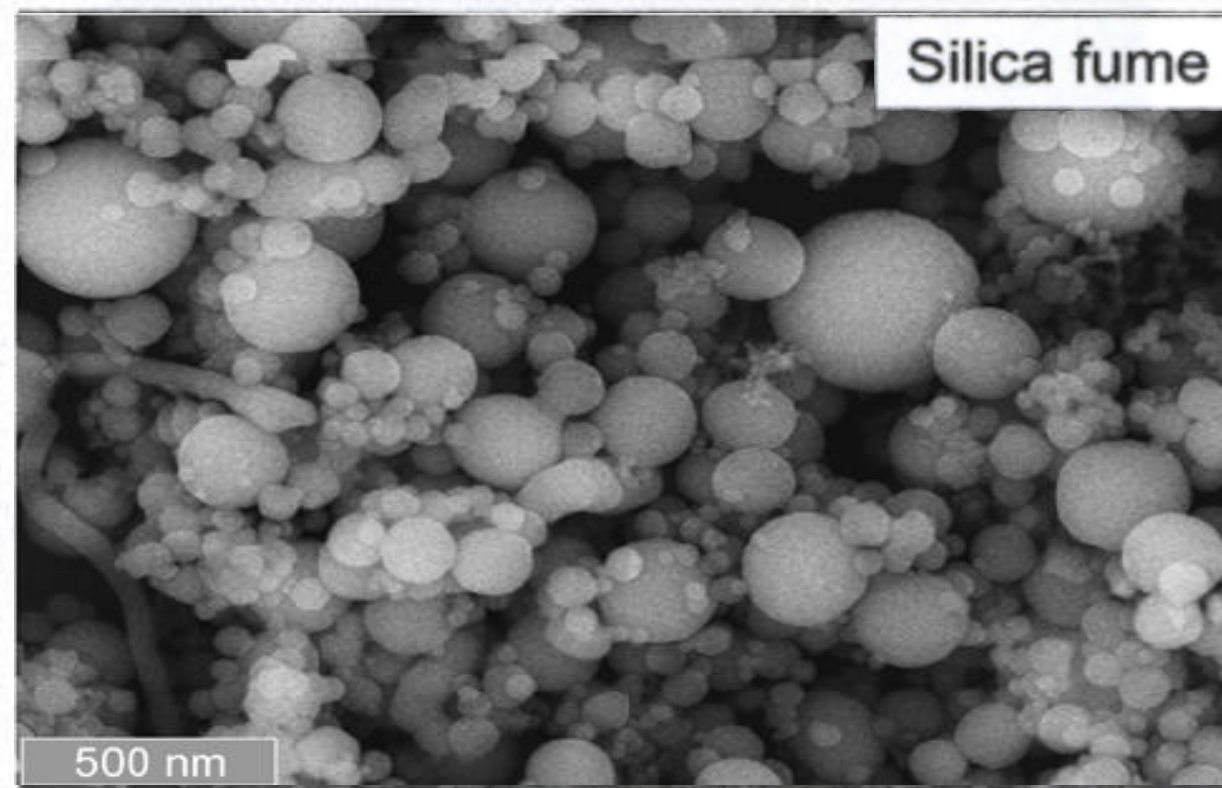
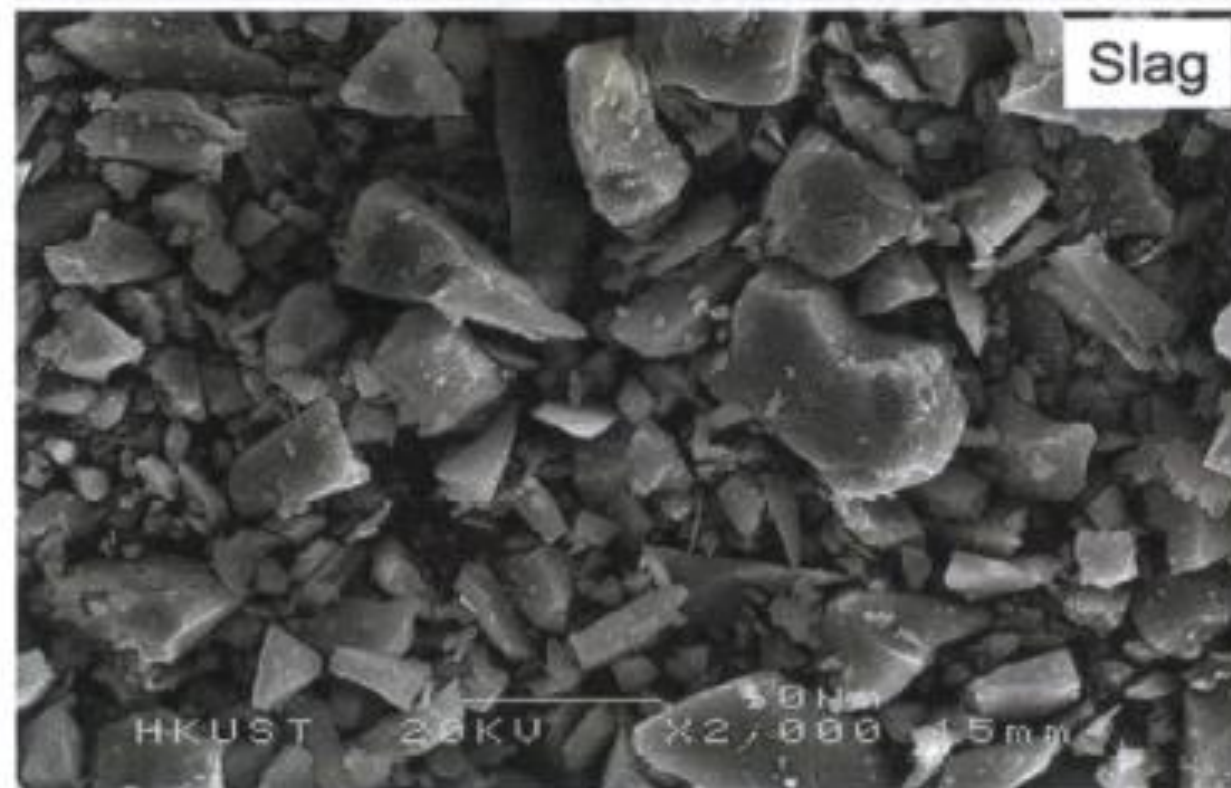
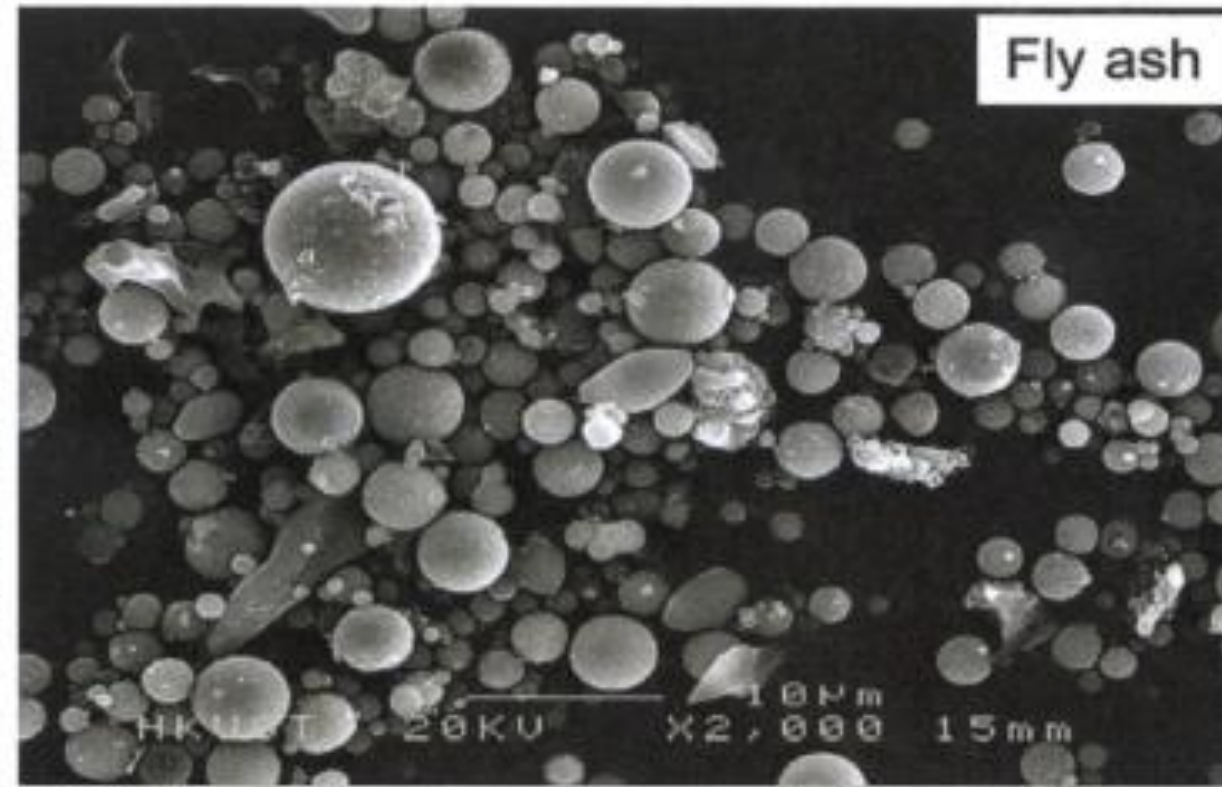
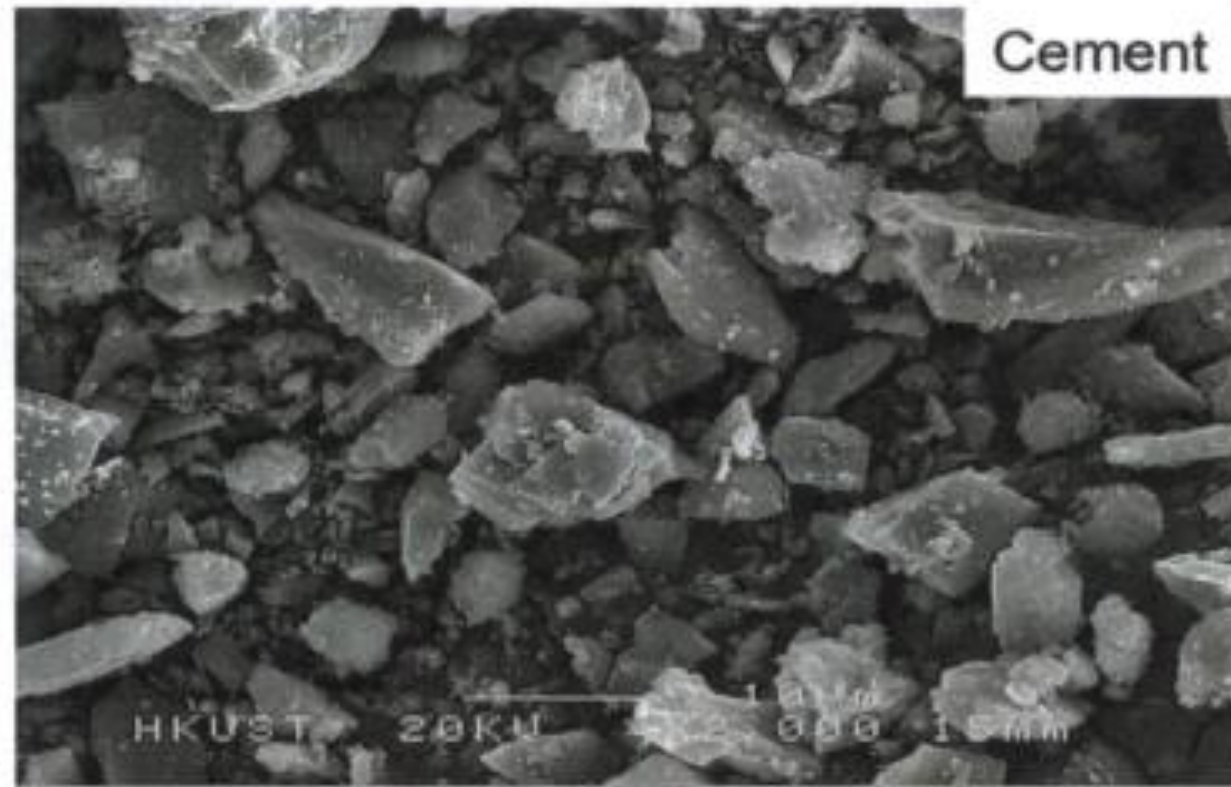
Produced during the process of converting molten iron from a blast furnace into steel in a converter

- **Electric-Arc-Furnace Slag (EAFS)**

Production process of melting scrap steel at high temperatures using an electric arc furnace, where scrap steel is the primary raw material, is known as electric arc furnace slag.

Binding Materials

- The following materials are normally used to produce a robust paste



Chemical Composition Of SCM-GGBS

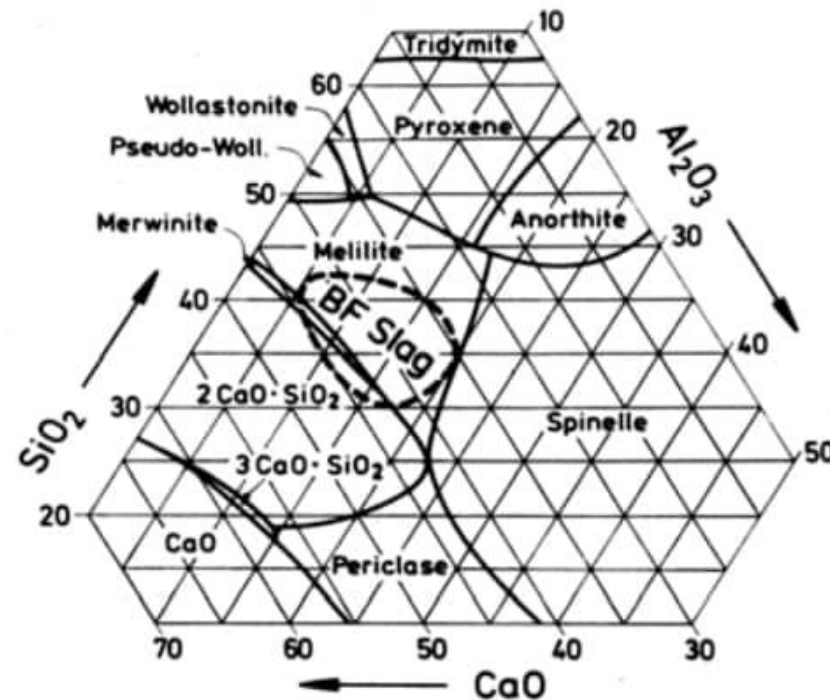
Range for Chemical Composition of Slag		
Composition	Usual range	Typical range
Silicon Dioxide (SiO ₂)	30–45	36
Aluminum Oxide (Al ₂ O ₃)	8–20	16.0
Calcium Oxide (CaO)	35–50	43.3
Magnesium Oxide (MgO)	0–20	7
Ferrous Oxide (FeO)	0–1.6	0.4
Sulfide sulfur (S)	0–2	1.5
Manganese Oxide (Mn ₂ O ₃)	0–2.5	< 0.1

Graphical Representation of Chemical Composition of Slag

Amorphous Content > 90 % (Best 95%)

$$\frac{\text{CaO} + \text{MgO} + \frac{1}{3} \text{Al}_2\text{O}_3}{\text{SiO}_2 + \frac{2}{3} \text{Al}_2\text{O}_3} \geq 1.0$$

Total amount of SiO₂+MgO+CaO>66%



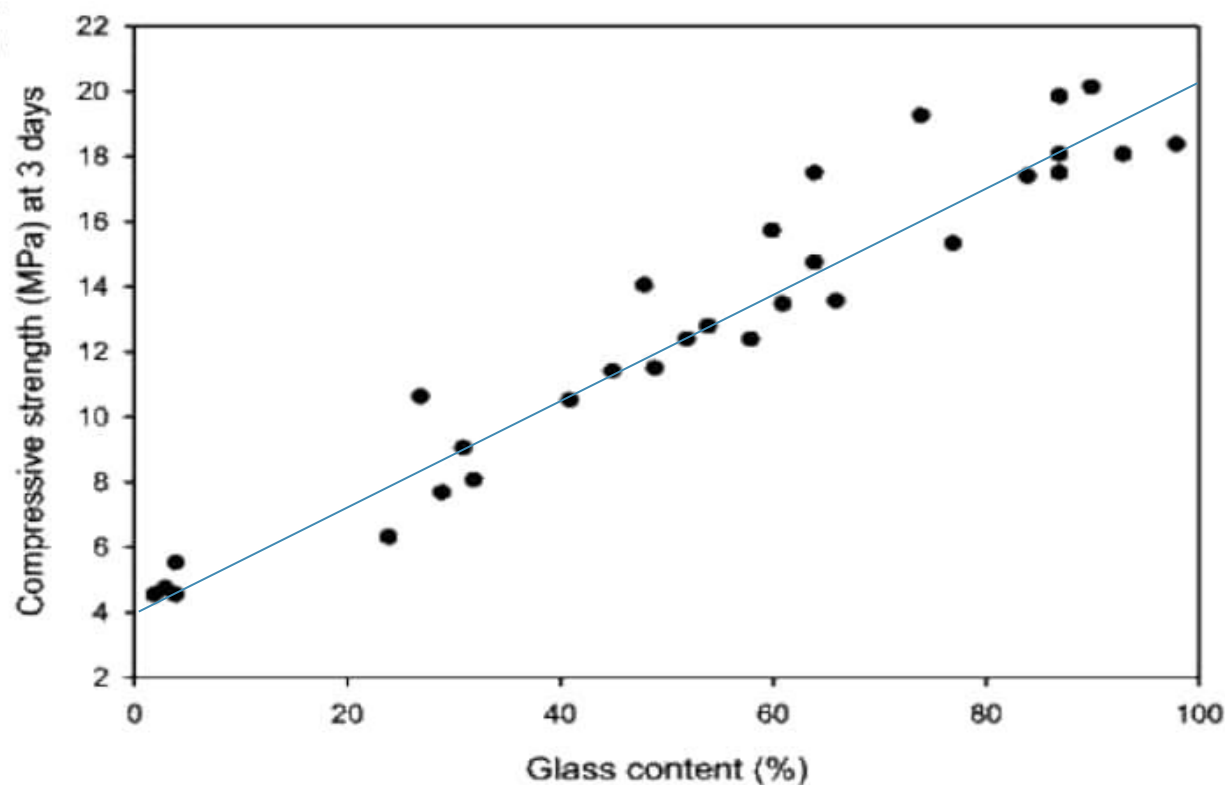
By-products: sustainability in society

As the glass phase content constitutes one of the essential features of slag, various methods have been proposed for measuring the degree of crystallinity.

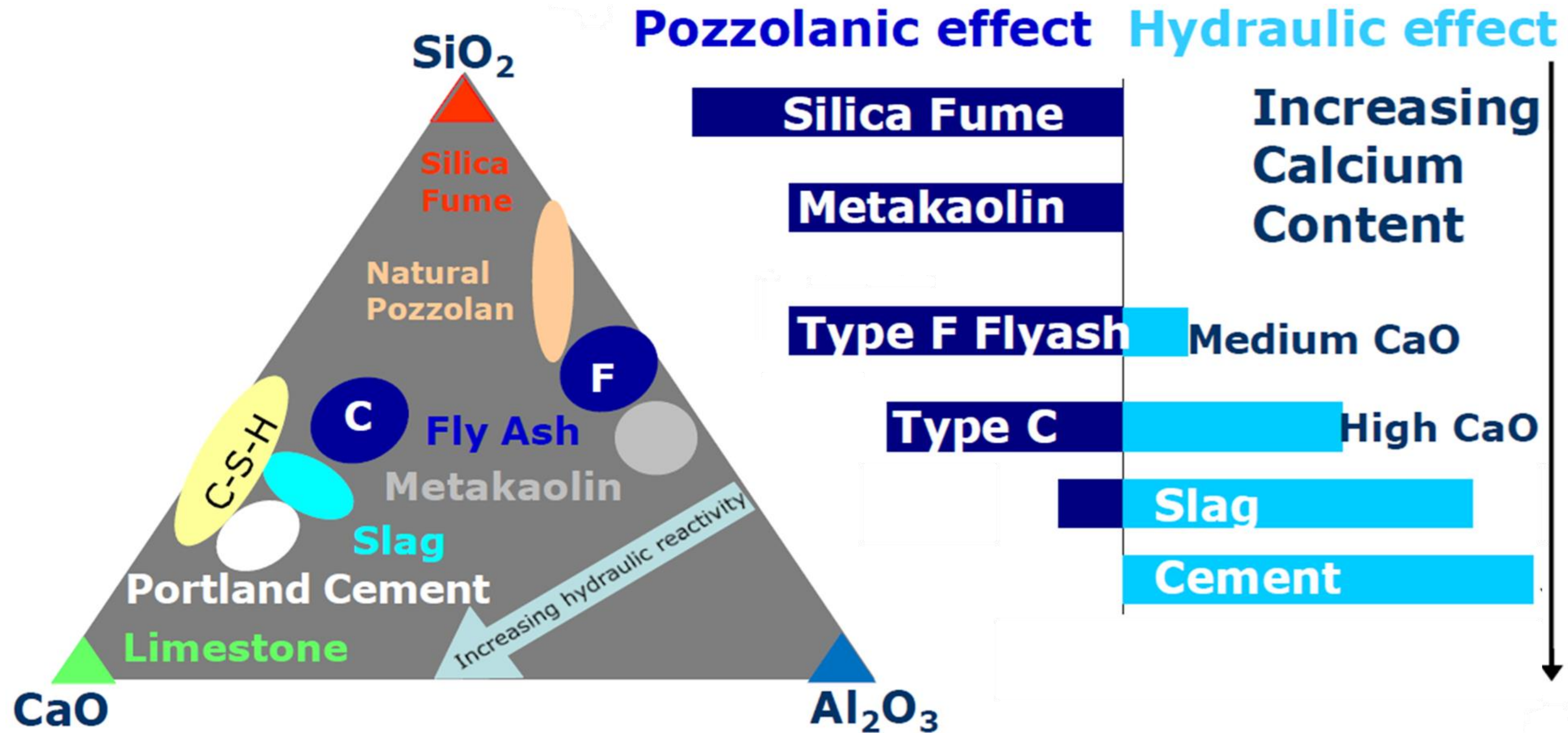
Owing to stress birefringence, it is difficult to distinguish between the crystalline phase and the stressed glassy phase.

From SEM, it is found that potassium and sulphur are localized mainly in the glass and that distribution of the elements is revealed.

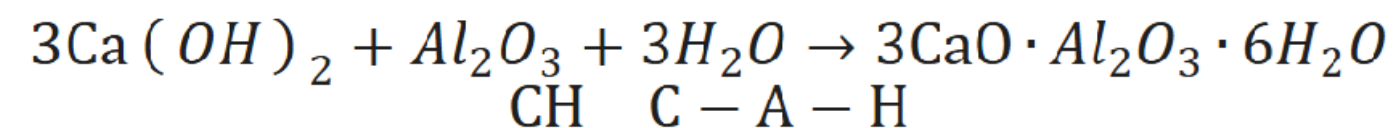
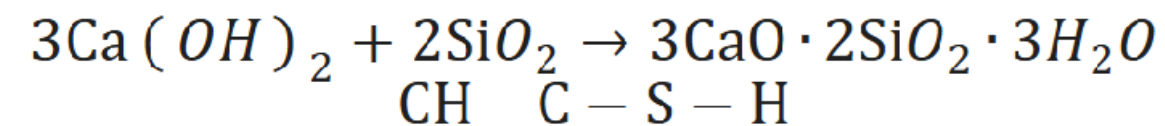
With reference to crystalline phases, it has recently been shown that the richer the slag is in akermanite, the less readily it hydrates.



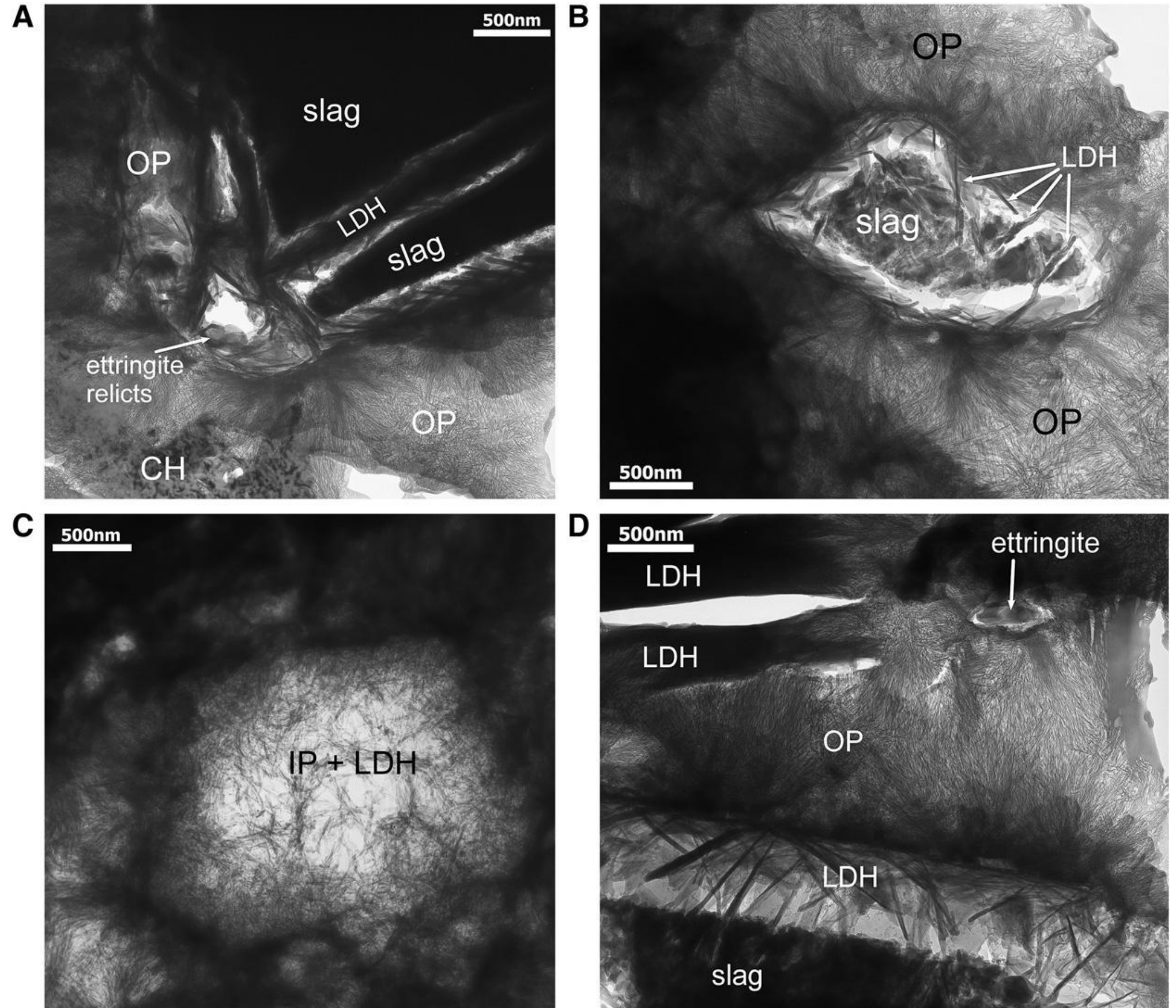
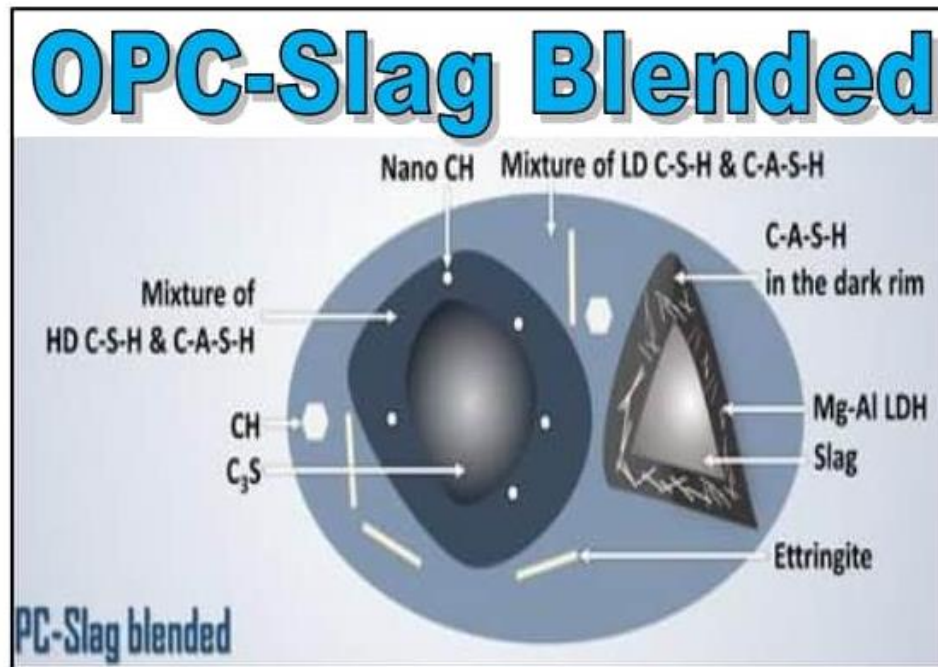
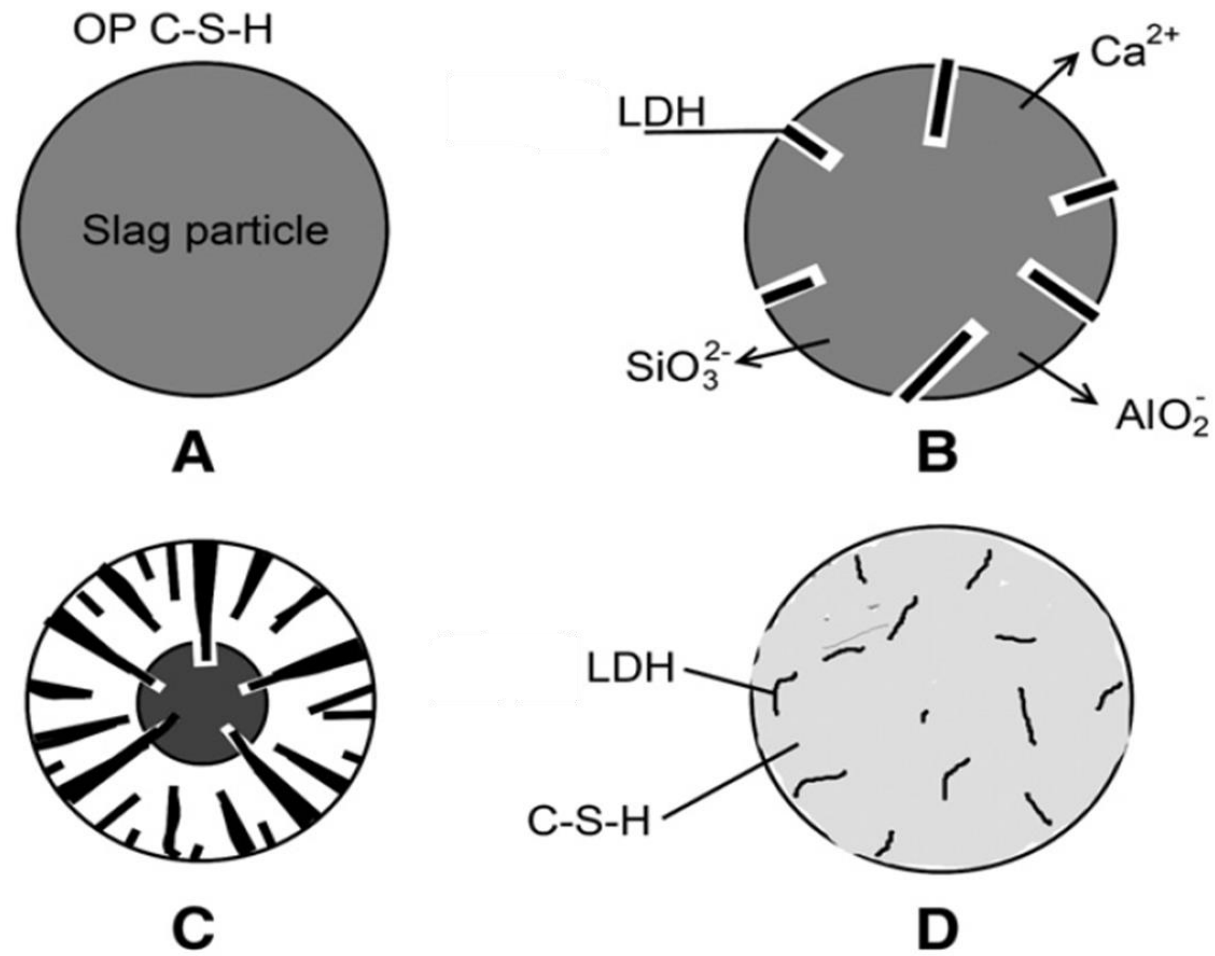
Binding Materials



- The pozzolanic reaction refers to the reaction of amorphous SiO_2 and Al_2O_3 with $\text{Ca}(\text{OH})_2$, resulting in the formation of C-S-H and C-A-H gel



Hydration Products of GGBS with OPC



Oversea Applications of GGBS – Concrete

- Discovered in Germany, 1862 and first commercially produced in 1865.
- GGBS was used in Europe and North America for over 100 years.
- Currently, GGBS has been widely used, particularly in China, Japan, Europe and USA.

Experience of Using GGBS in Concrete

Region	GGBS Usage
Western Europe	<ul style="list-style-type: none">• GGBS accounts for about 20% of total cement consumed
Netherlands	<ul style="list-style-type: none">• GGBS accounts for 60% of total cement consumption
USA	<ul style="list-style-type: none">• Concrete in World Trade Centre construction has about 40% GGBS replacement
	<ul style="list-style-type: none">• Georgia Aquarium used 20% to 70% GGBS replacement
	<ul style="list-style-type: none">• Metro Airport Terminal Expansion used concrete with 30% GGBS replacement
China	<ul style="list-style-type: none">• GGBS widely used in major projects like Three Gorges Dam, Beijing-Shanghai Express Rail, and Hangzhou Bay Bridge
Singapore	<ul style="list-style-type: none">• Launch national standard in 2008
Hong Kong	<ul style="list-style-type: none">• Tsing Ma Bridge construction with GGBS replacement levels between 59% and 65%
	<ul style="list-style-type: none">• Stonecutter Island Bridge construction with GGBS replacement between 60% and 70%

Specification Standard in Hong Kong

BS EN 15167-1:2006

Property		Requirements for GGBS
Physical Properties		
Moisture Content		<1.0%
Density		-
Fineness		≥275m ² /kg
Initial Setting Time		S1 ≤ 2 x S2
Activity Index	7-day age	≥45%
	28-day age	≥70%
Chemical Properties		
Magnesium Oxide (MgO)		≤18%
Sulfide (S ²⁻)		≤2.0%
Sulfate (SO ₃)		≤2.5%
Loss on ignition, corrected for oxidation of sulfide		≤3.0%
Chloride (Cl ⁻)		≤0.10%

Specification Standard in GBT

GB/T 18046-2017

Property		Requirements for GGBS			EN 15167-1:2006
		S105	S95	S75	
Physical Properties					
Density		≥2.8g/cm ³			
Fineness – Blaine		<500m ² /kg	<400m ² /kg	<300m ² /kg	≥275m ² /kg
Active Index	7days	≥95	≥70	≥55	≥45%
	28days	≥105	≥95	≥75	≥70%
Fluidity Ratio		≥95			
Water Ratio		≤1.0			
Chemical Properties					
Sulphur Trioxide		≤4.0%			
Chloride Ion		≤0.06%			
Loss on Ignition		≤1.0%			
Insoluble Content		≤3.0%			



2. APPLICATION OF GGGBS IN CONCRETE –

- PROS & CONS AND SOLUTIONS

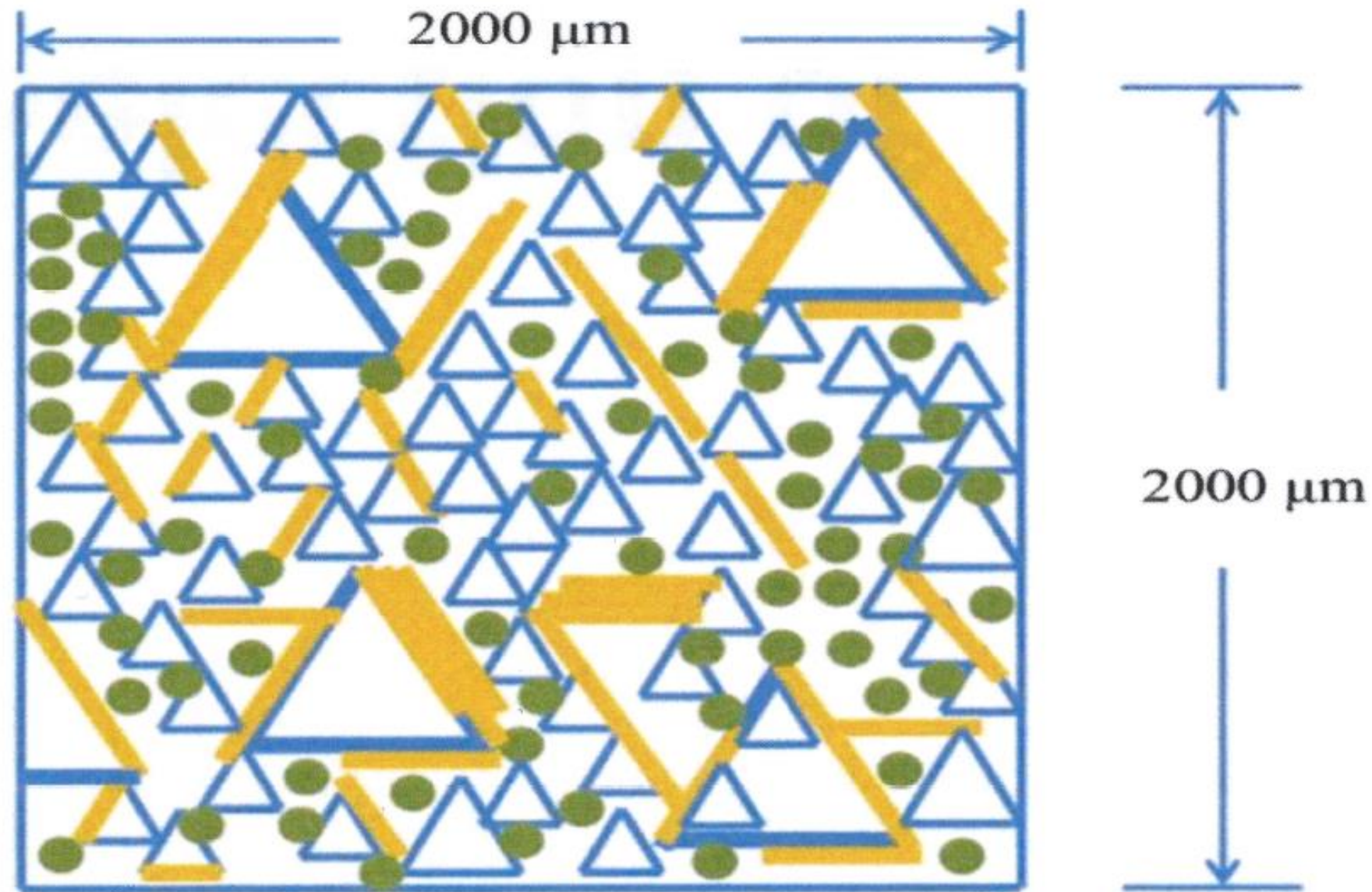
Advantages in performance

- Reducing water permeability
- Increasing corrosion resistance
- Lower peak temperature
- Better AAR Resistance

Disadvantages in performance

- Prolonged setting time
- Drying Shrinkage
- Lower early strength at initial hardening stage

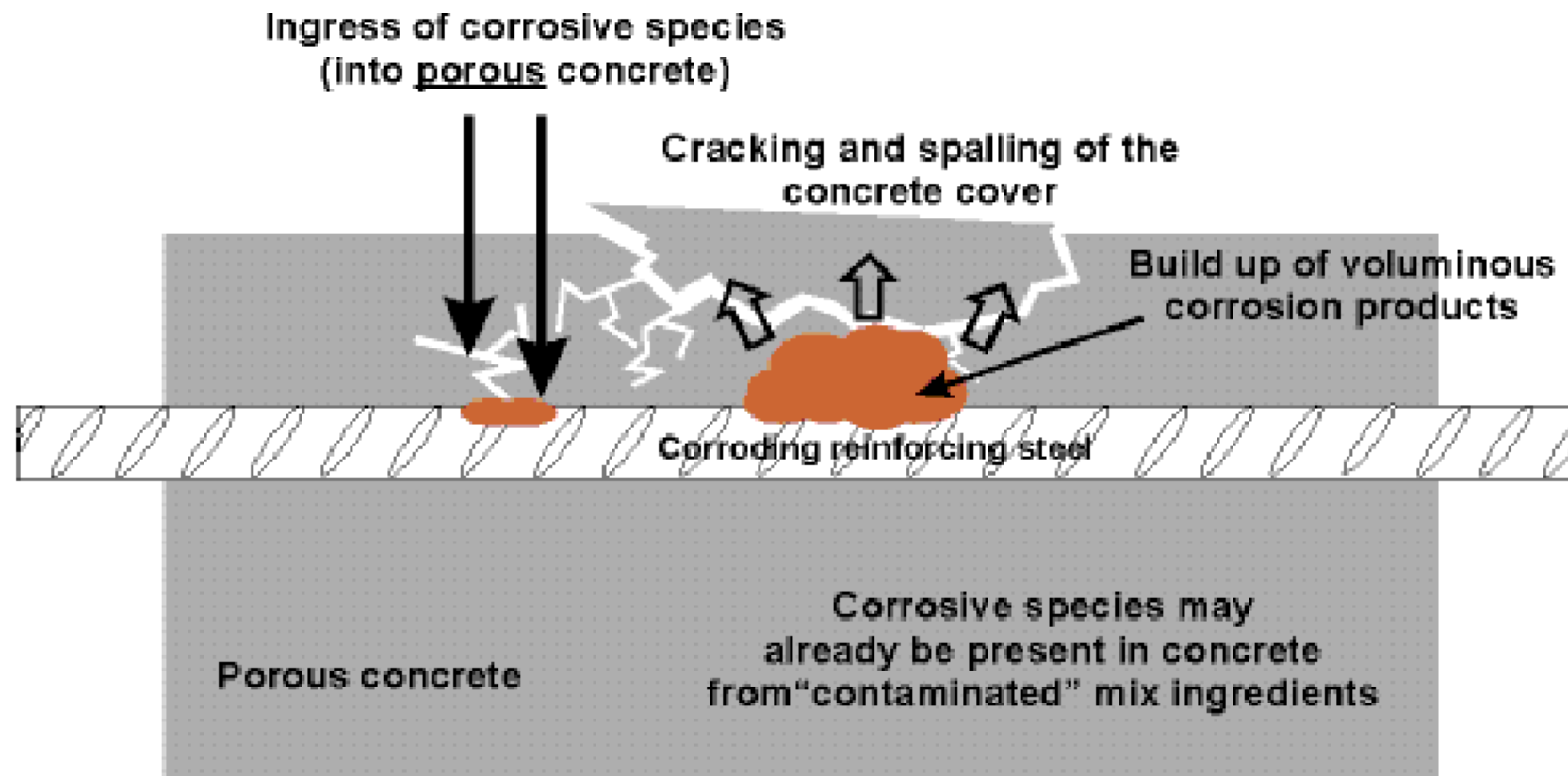
Reducing Water Permeability



- The permeability of concrete is an important characteristic of durable concrete, and concrete with a reduced water penetration depth shows significant resistance to chemical assaults
- Less voids tend to cause a decrease in the permeability of concrete.
- Concrete with a lower permeability is more resistant to chemical attack, including chloride, sulphate, AAR and acid.

Resistance of Chemical Attack

- Chloride attack is a major threat to concrete durability, causing around 40% of concrete building failures.
- The reaction of GGBS with calcium hydroxide and alkalis during hydration fills the pores with calcium silicate hydrates, improving durability against chloride penetration.



Resistance of Chemical Attack

GGBS Concrete Plant Trial with RCPT Test on 14 July 2022

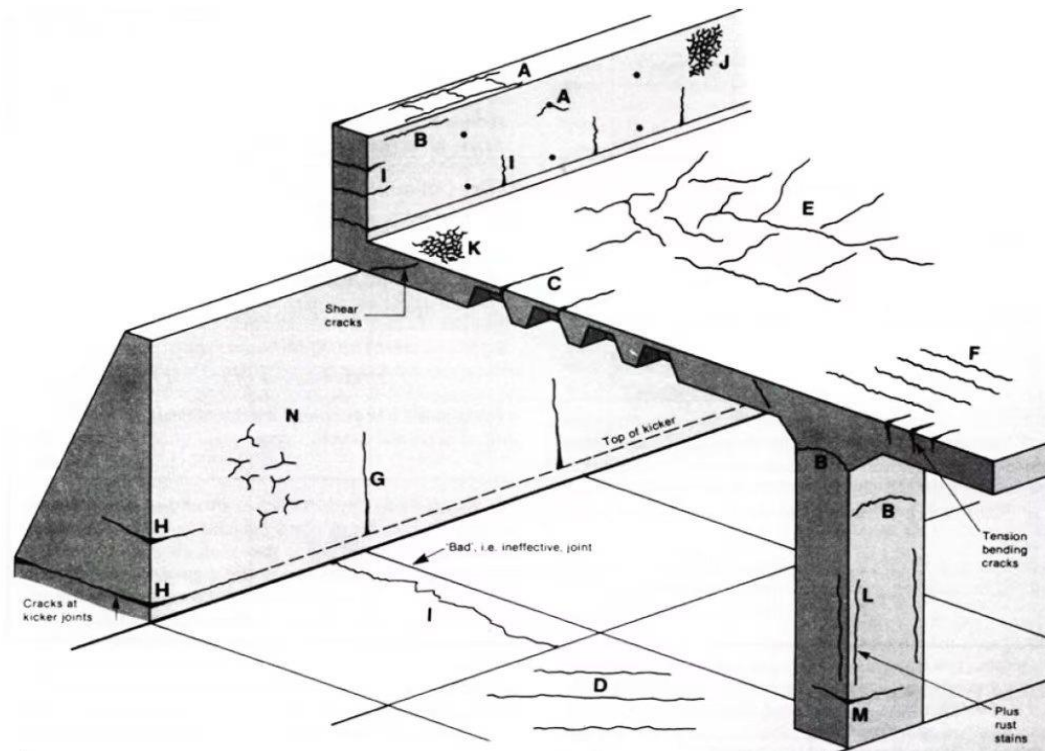
<u>Mix</u>		<u>Design</u>	<u>Compressive Strength (MPa)</u>						
			<u>1 Days</u>	<u>2 Days</u>	<u>4 Days</u>	<u>7 Days</u>	<u>14 Days</u>	<u>28 Days</u>	
<u>Code</u>	<u>Mix</u>	<u>Slump</u>	<u>Cube</u>	<u>Cube</u>	<u>Cube</u>	<u>Cube</u>	<u>Cube</u>	<u>Cube</u>	<u>RCPT Test (Coulombs)</u>
C45 60% GGBS+ CSF	45/20D (0.36wc)	600 Flow	14.6	27.5	40	54.5	67.3	79	89
C60 65% GGBS	60/20D (0.35wc)	200	15	29	42.5	57.5	73	80	617
C45 65% GGBS	45/20D Tremie (0.39wc)	200	-	15	28	45.5	64.35	78.5	890

- RCPT test result for OPC concrete(C45) at 28 days is about 2500 Coulombs
- Adding GGBS can lower the result to less than 900 Coulombs



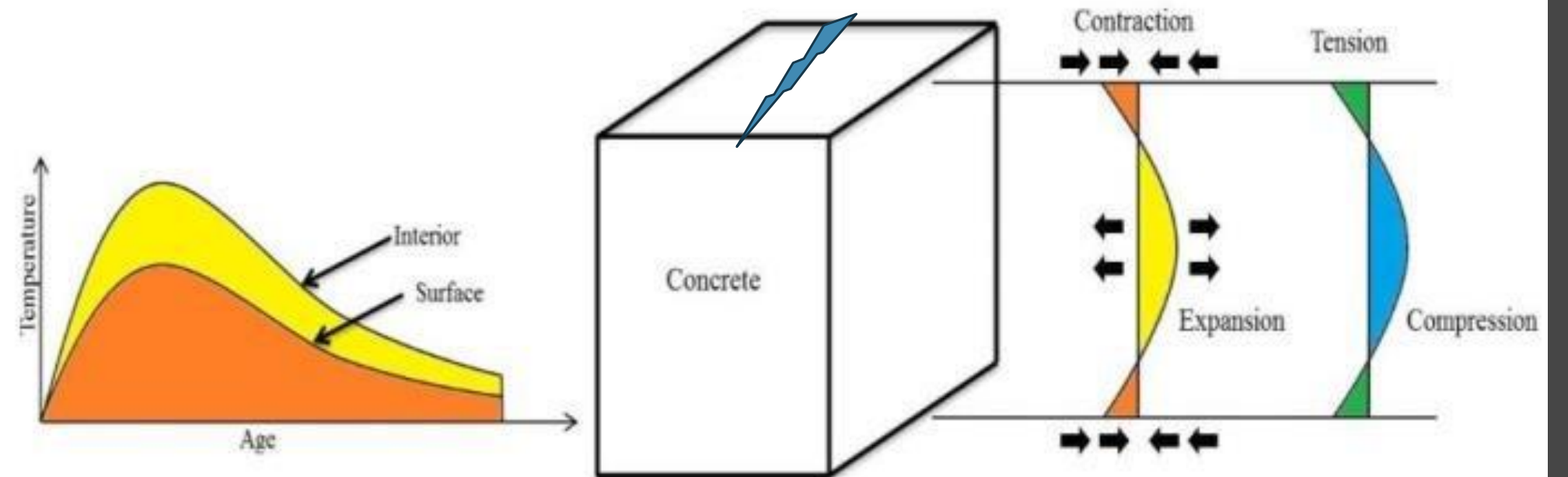
Lower Peak Temperature

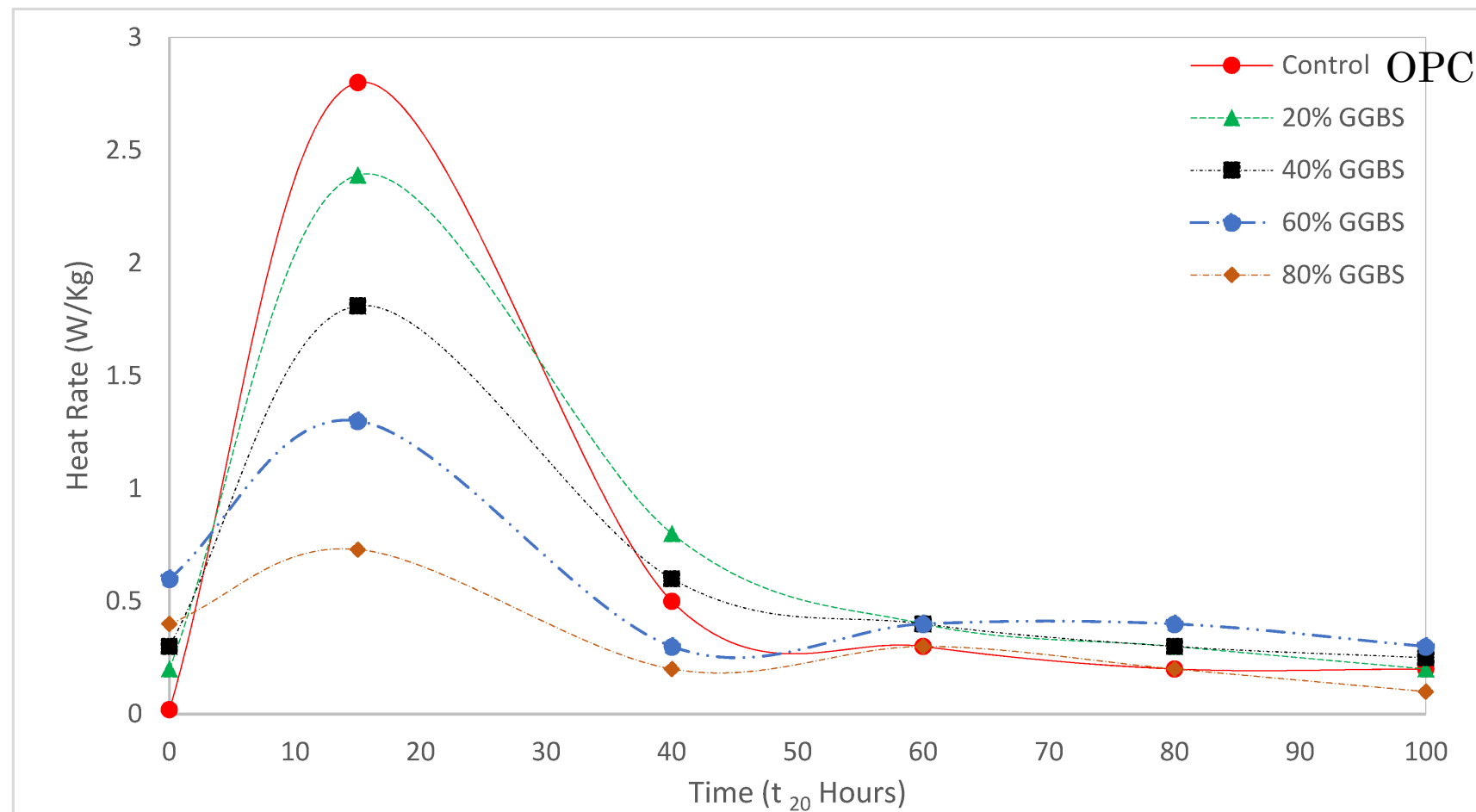
- Primary causes of thermal cracking in concrete due to **temperature differentials**. Variations in temperature across the concrete structure can result in thermal gradients. When different parts of the concrete expand or contract at different rates due to temperature changes, internal stresses can build up, leading to cracking.



Letter	Type of Cracking	Subdivision	Most Common Location	Primary Cause (excluding restraint)	Secondary Causes/Factors	Time of Appearance
A	Plastic settlement	Over reinforcement	Deep sections	Excess bleeding	Rapid early drying conditions	Ten minutes to three hours
B		Arching	Top of columns			
C		Change of depth	Trough and waffle slab			
D	Plastic shrinkage	Diagonal	Roads and slabs	Rapid early drying	Low rate of bleeding	Thirty minutes to six hours
E		Random	Reinforced concrete slabs			
F		Over reinforcement	Reinforced concrete slabs			
G	Early thermal contraction	External restraint	Thick walls	Excess heat generation	Rapid cooling	One day or two or three weeks
H		Internal restraint	Thick slabs	Excess temperature gradients		
I	Long-term drying shrinkage		Thin slabs (and walls)	Inefficient joints	Excessive shrinkage inefficient curing	Several weeks or months
J	Crazing	Against formwork	"Fair faced" concrete	Impermeable formwork	Rich mixes	One to seven days, sometimes much later
K		Floated concrete	Slabs	Over troweling		
L	Corrosion of reinforcement	Natural	Columns and beams	Lack of cover	Poor quality concrete	More than two years
M		Calcium chloride	Precast concrete	Excess calcium chloride		
N	Alkali-aggregate reaction		Damp locations	Reactive aggregate plus high-alkali cement		More than five years

Example of thermal cracking





- The pozzolanic reaction continues gradually and is associated with the hydration of cement, which ultimately causes a decline in the heat, especially in the early days of hydration. Resulting lower peak temperature in GGBS concrete.

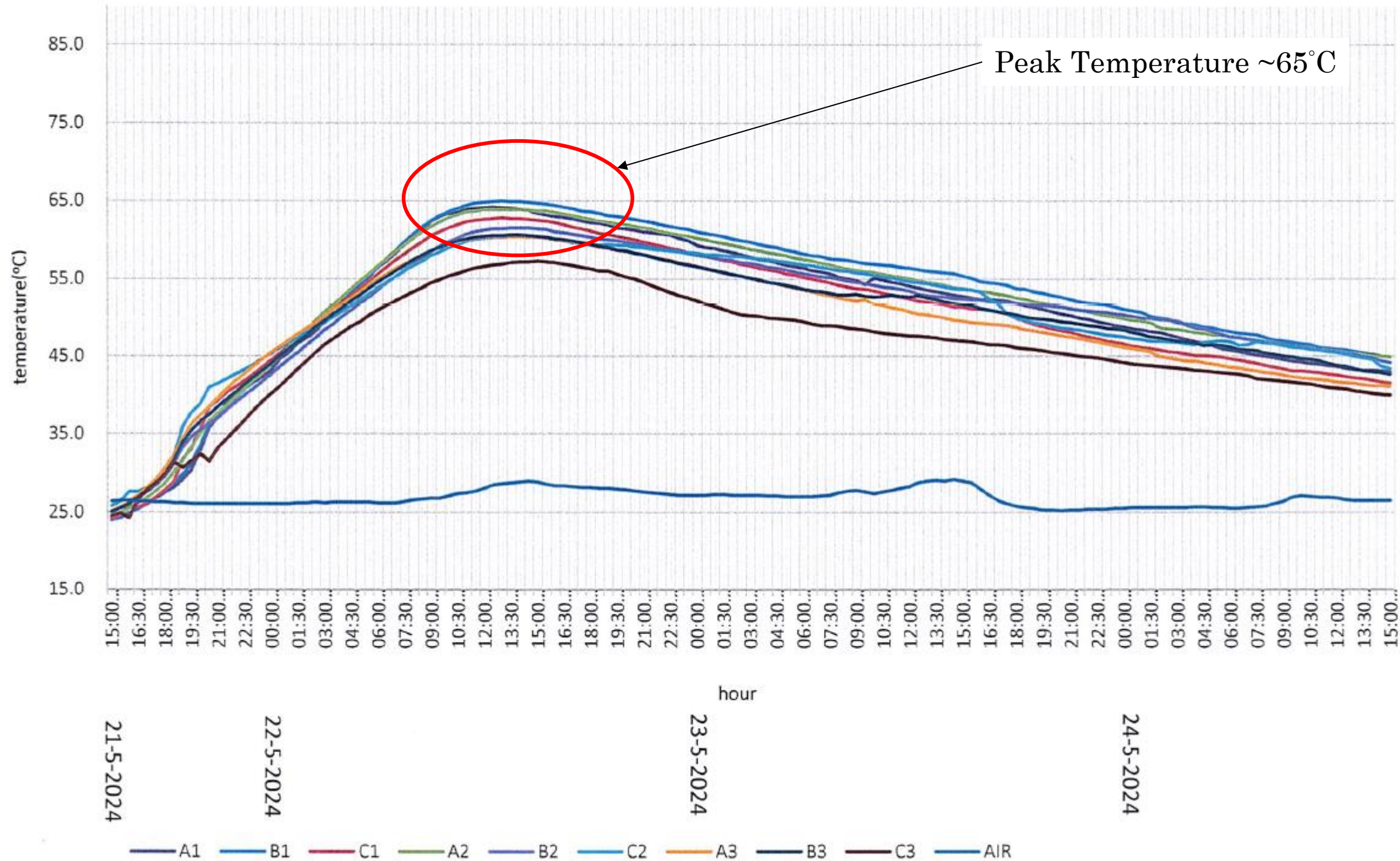
Reactions of Principal Clinker Phases



Lower Peak Temperature

Project: Cameron Road - Temperature Rise Evaluation
Location: Trial Column
Concrete Mix: D80/20 50%GGBS+CSF TC 30°C
Test Date: 21-24/5/2024

Temperature Monitoring- Trial Column



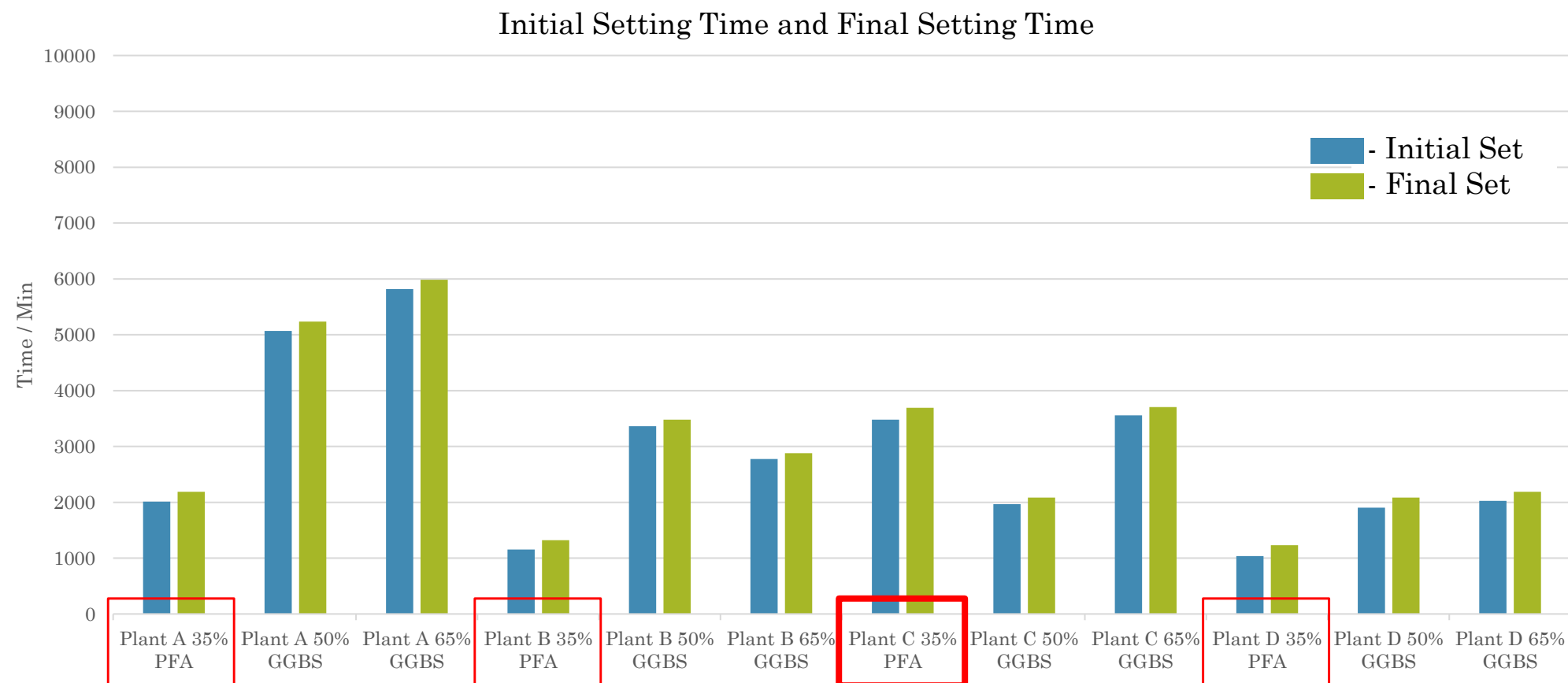
Lower Peak Temperature

D80/20 50%GGBS+CSF				
Cement	244			
GGBS	277			
CSF	33			
20 mm	670			
10 mm	315			
S/F	690			
Water	155			
w/c	0.28			
Slump Retention				
initial	220		220	
1 hr	210		205	
Compressive Strength (MPa) (150mm)				
7 Days	77.1	80.9	78.8	74.5
28 Days	86.9	87.5	88.9	86.6

Prolonged Setting Time at Fresh Stage

GGBS & PFA tremie concrete research by MTR (2024)

Setting Time



- The concrete mixes showed stiffening times exceeding 10 hours, enabling ample time for delivery and placement in tremie construction. GGBS mixes, except for plant C, displayed **longer setting times than PFA mixes**, showcasing GGBS's ability to extend setting times for tremie construction.
- These results emphasize the adaptability of GGBS mixes, underscoring the importance of adjusting admixture content to meet specific construction requirements.

Prolonged Setting Time at Fresh Stage

Bored Pile				
	D45 25%PFA	D45 60%GGBS	D60 25% PFA	D60 60%GGBS
Cement	402	184	405	200
PFA	134	0	135	0
GGBS	0	276	0	300
Water	205	200	180	200
w/c	0.38	0.43	0.33	0.40
Slump Retention				
initial	220	220	230	230
1 hr	220	220	230	230
2 hrs	210	210	220	230
10 hrs	120	150	130	160
Stiffening Time (20°C)				
Initial set (hr)	24	26	24	25
Final set (hr)	28	30	28	30
Compressive Strength (MPa)				
7 Days	45	48	59	54
28 Days	60	62	78	81

Prolonged Setting Time at Fresh Stage

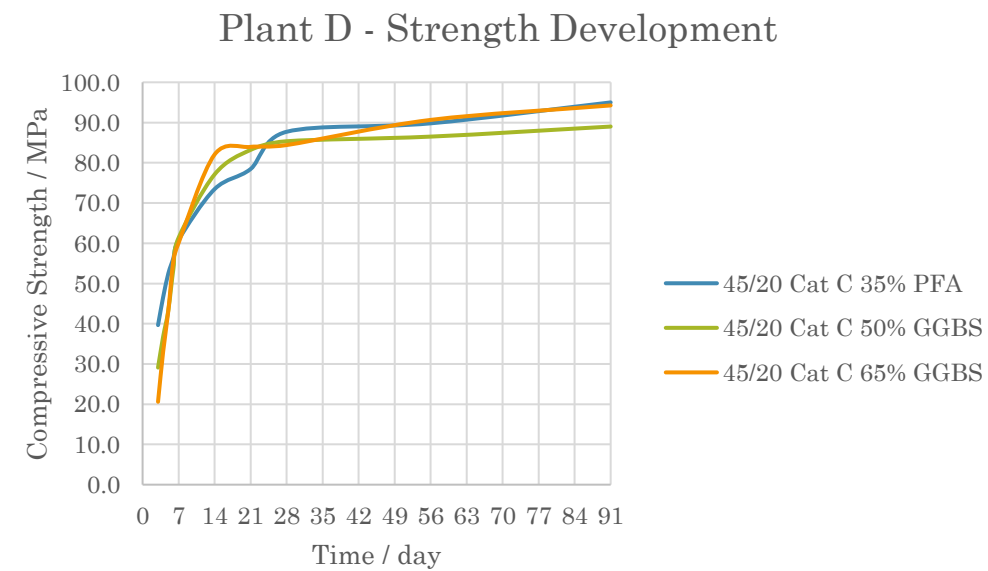
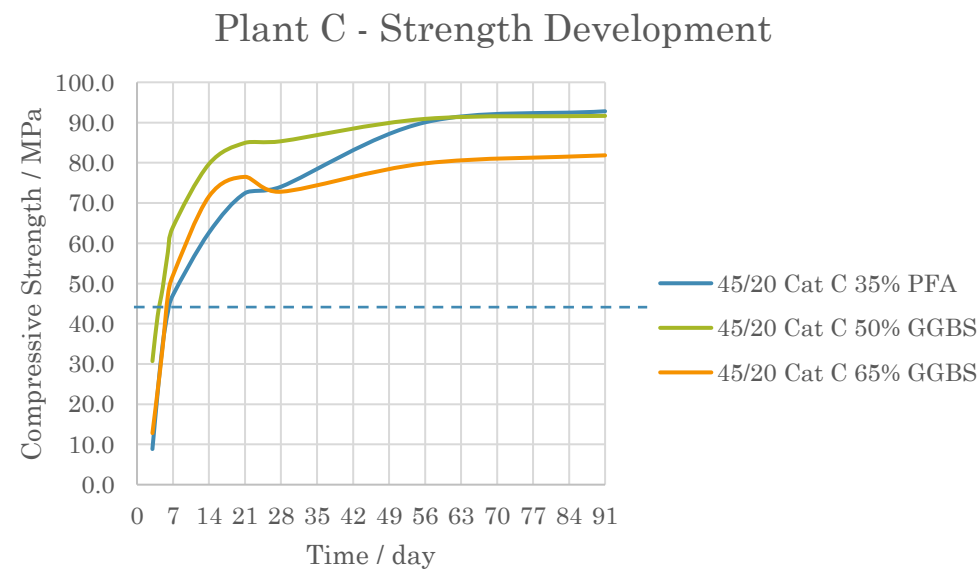
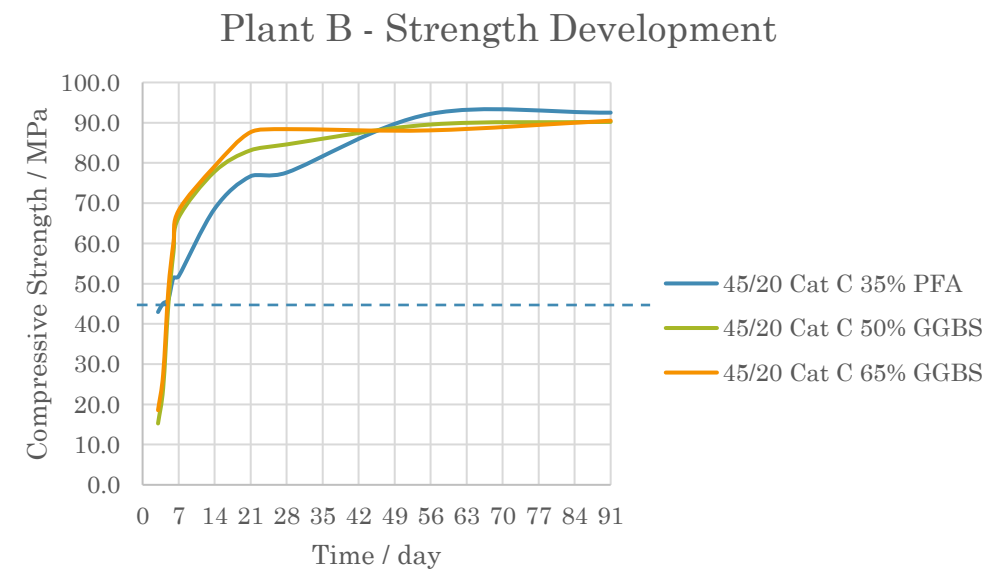
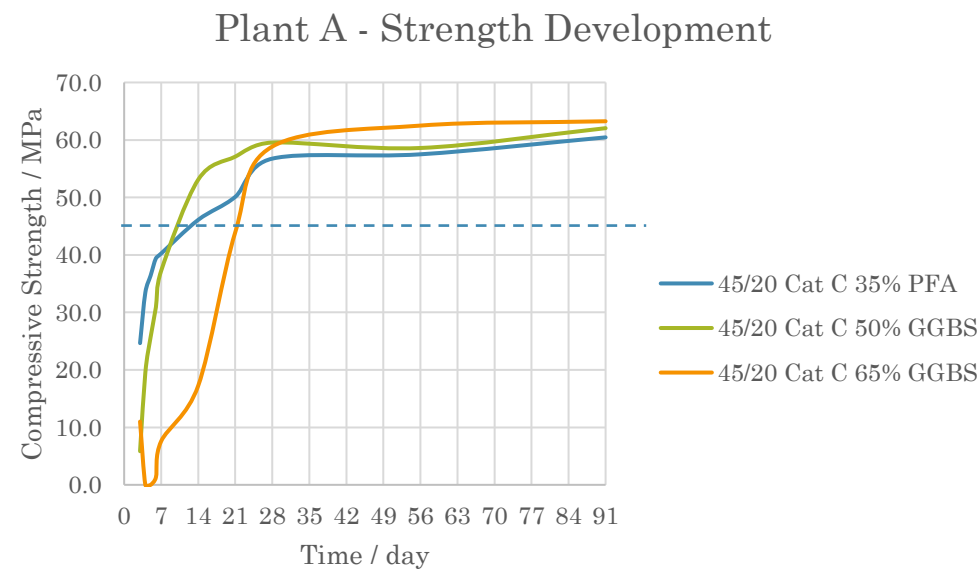
Pile Cap				
	D40 35%PFA	D40 65%GGBS	D45 35%PFA	D45 65%GGBS
Cement	325	140	338	154
PFA	175	0	182	0
GGBS	0	260	0	286
Water	207	200	197	200
w/c	0.41	0.50	0.38	0.45
Slump Retention				
initial	180	180	180	180
1 hr	160	170	160	160
Stiffening Time (20°C)				
Initial set (hr)	9	10	8	10
Final set (hr)	11	12	10	12
Compressive Strength (MPa)				
7 Days	36	34	40	37
28 Days	53	55	60	62

Prolonged Setting Time at Fresh Stage

Normal Concrete						
	D45 OPC	D45 45%GGBS	D45 25% PFA	D60 OPC	D60 45%GGBS	D60 25% PFA
Cement	440	242	330	500	264	375
PFA	0	0	110	0	0	125
GGBS	0	198	0	0	216	0
Water	198	200	175	170	170	165
w/c	0.45	0.45	0.40	0.34	0.35	0.33
Slump Retention						
initial	180	180	180	220	220	220
1 hr	150	160	160	200	210	210
Stiffening Time (20°C)						
Initial set (hr)	6	8	7	6	7	6
Final set (hr)	8	10	9	7	9	8
Compressive Strength (MPa)						
7 Days	46	49	43	64	53	60
28 Days	61	67	59	81	85	77

GGBS & PFA tremie concrete research by MTR

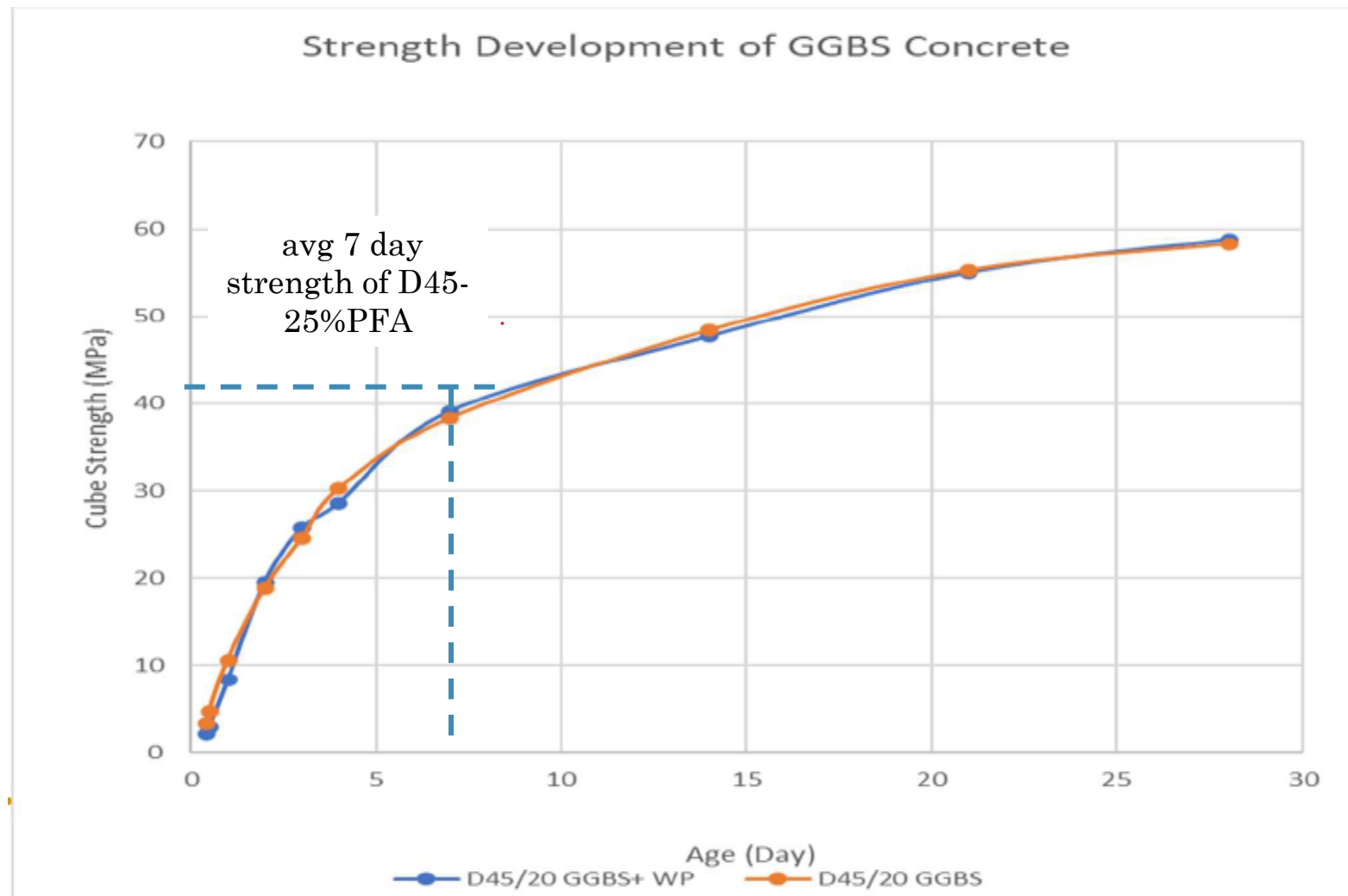
Strength Development



- An observable trend indicated that the initial strength of PFA mixes typically better than that of GGBS mixes, predominantly attributed to the lower dosage of 35% PFA. Strength evolution persisted up to 28 days, with marginal enhancements observed up to 91 days.
- Noteworthy the difference in strength between the 35% PFA, 50% GGBS, and 65% GGBS mixes was insignificant within each supplier.

Lower Early Strength at Initial

Mix Description	Slump	Cement	GGBS	20mm	10mm	Fine	Water	Retarder	Superplastizer	Concreteproof	A/C	W/C
D45 45%GGBS	150	242	198	610	270	800	200	2.00-4.50	2.50-4.50		3.82	0.45
D45 45%GGBS WP	150	242	198	610	270	800	200	2.00-4.50	2.50-4.50	1.54	3.82	0.45



- 17/4/2023 King Lam Street

Lower Early Strength at Initial

Mix Design – D60/20 45%GGBS

Science Park 12W-A

M/F beam / Signal 1

Report generated on Mar 12th, 2024 by Lai Chi Sing

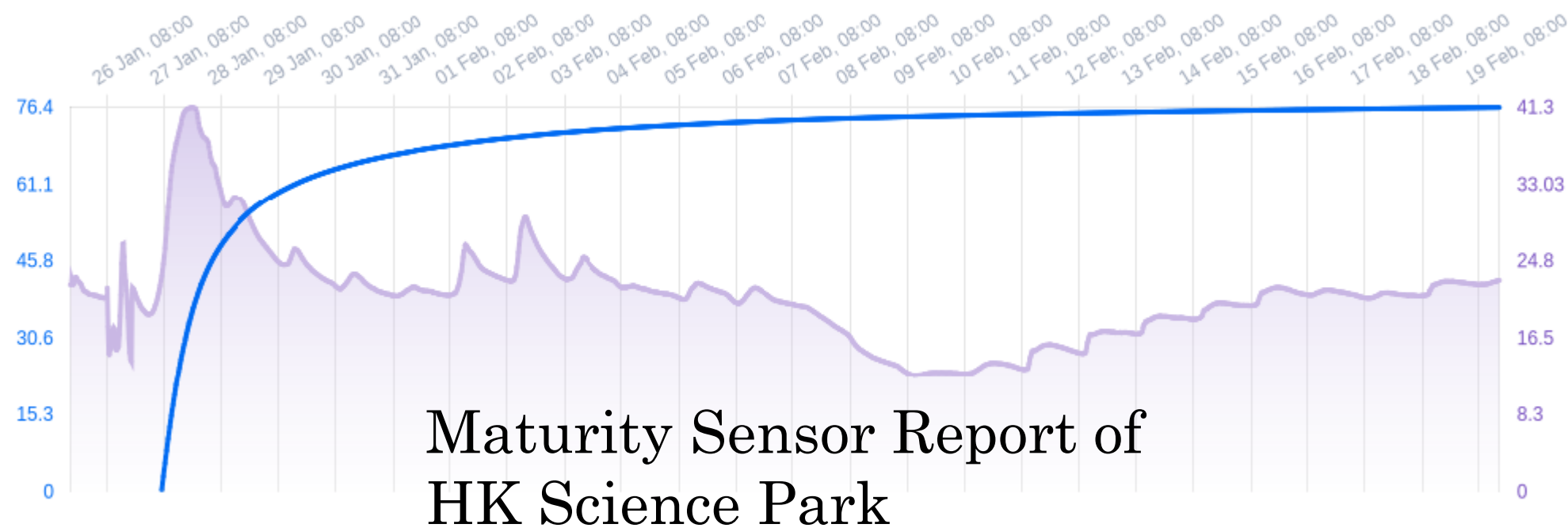
76.4MPa
Compressive Strength
Feb 19th, 2024, 16:36

22.7°C
Temperature
Feb 19th, 2024, 16:36

41.3°C
Highest Temperature
Jan 27th, 2024, 19:37

12.5°C
Lowest Temperature
Feb 9th, 2024, 10:36

Temperature & Strength over Time



Maturity Sensor Report of
HK Science Park

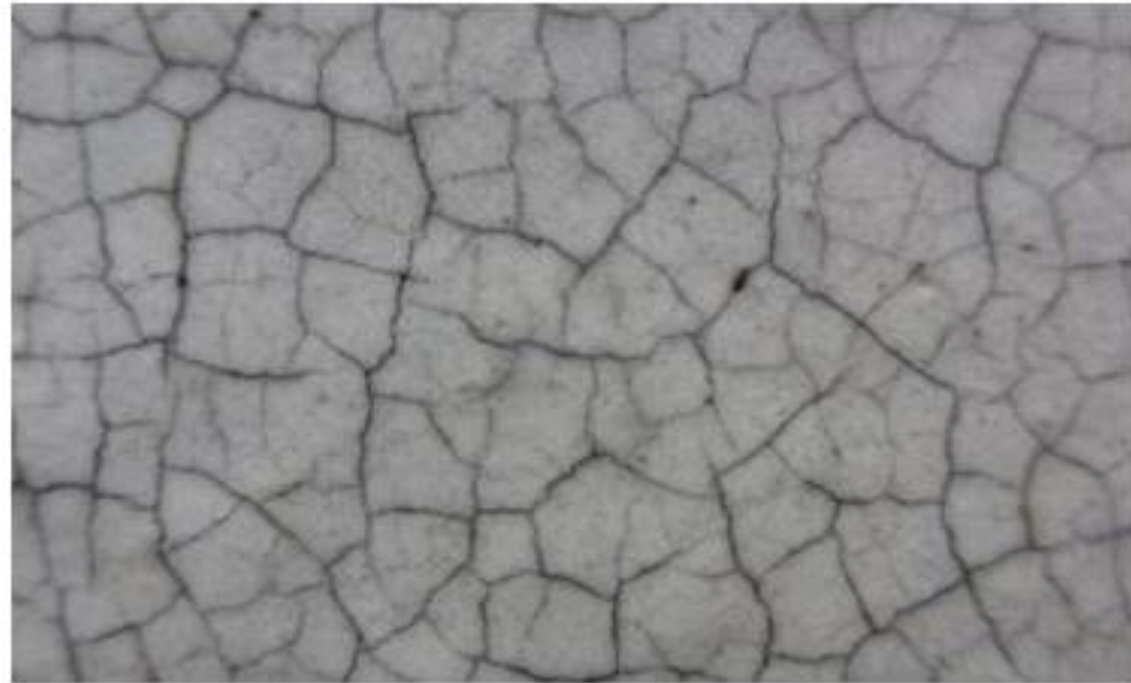
3 Days to achieved designed strength

Concrete Poured	Jan 26th, 2024, 19:45
30MPa	Jan 27th, 2024, 16:37
40MPa	Jan 27th, 2024, 22:37
50MPa	Jan 28th, 2024, 09:17
60MPa	Jan 29th, 2024, 10:17
Last Recorded Strength	Feb 19th, 2024, 16:36

Internal Cube Test Result Conducted in QH	
1days	20.9/20.1
2days	41.2/41.8
4days	55.1/54.4
7days	67.3/66.9
14days	75.7/73.9
21days	80.6/82.8
28days	86.7/85.0

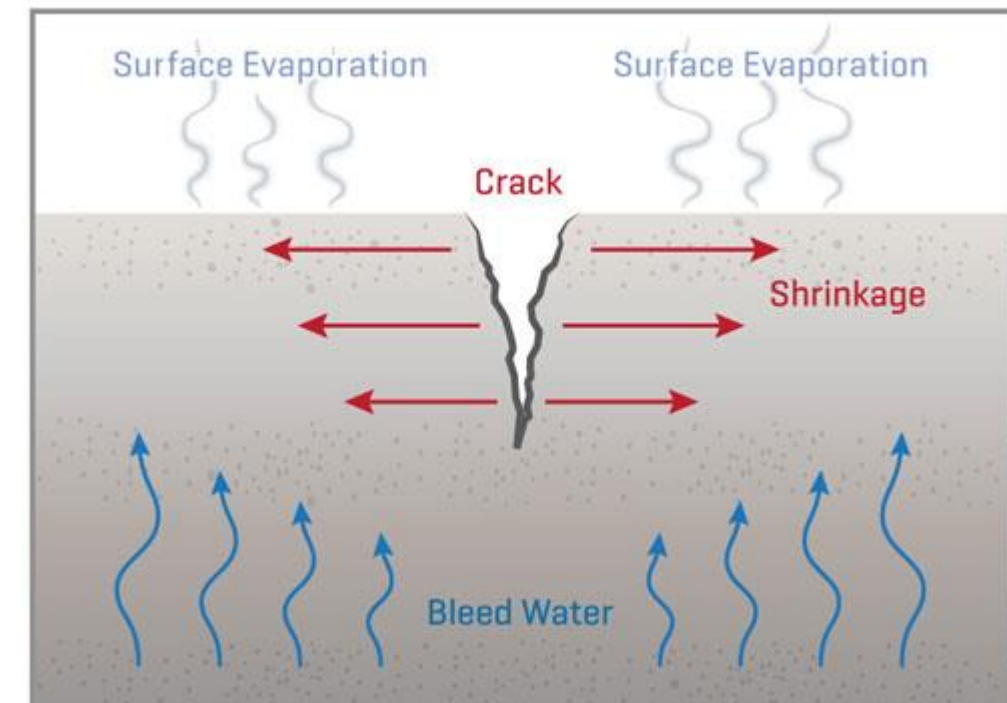
Plastic Shrinkage

- People claim early strength for concrete with GGBS is lower than that of OPC concrete, plastic shrinkage crack is prone to happen



CIVIL ENGINEERING DAILY ©

Plastic shrinkage is caused by the loss of water by evaporation from the surface of newly laid concrete or by suction of dry concrete underneath. At the surface, plastic shrinkage occurs when the rate of evaporation exceeds the rate of bleeding



Plastic Shrinkage

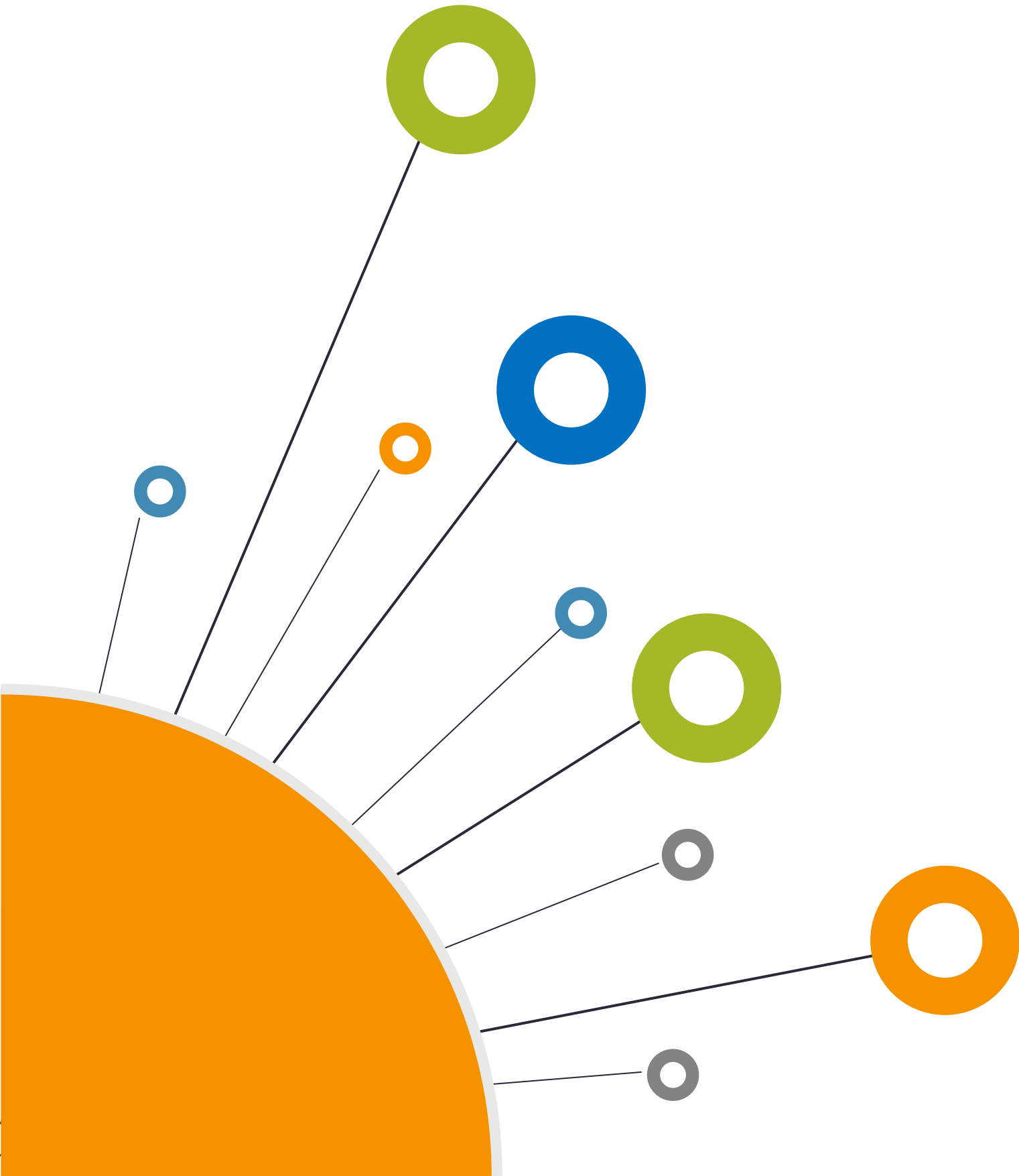
GGBS concrete under low temperature curing												
Concrete Grade	Compressive Strength											
	7-10°C				13-15°C				27°C			
	24 hrs	36 hrs	48 hrs	28 days	24 hrs	36 hrs	48 hrs	28 days	24 hrs	36 hrs	48 hrs	28 days
C45 Cementitious content:430 (OPC)	5	17.7	24.2	62.6	8.3	19.5	24.9	61	31.3	38.1	45.9	58.2
C45 Cementitious content:430 (OPC+25%PFA)	2.5	9.7	13.8	58.3	4.1	12.9	16.6	56.3	19	25.2	30.7	61.7
C45 Cementitious content:430 (OPC+45%GGBS)	4.7	8.5	13.4	60.6	7.4	10.1	14.2	61.6	18.6	23.4	29.5	61.5



- Local curing example - Pile Cap (16/10/2024)
- Proper curing by controlling **moisture** and **temperature** of in-situ concrete
- Adequate curing should be conducted for every concrete structure to avoid plastic shrinkage

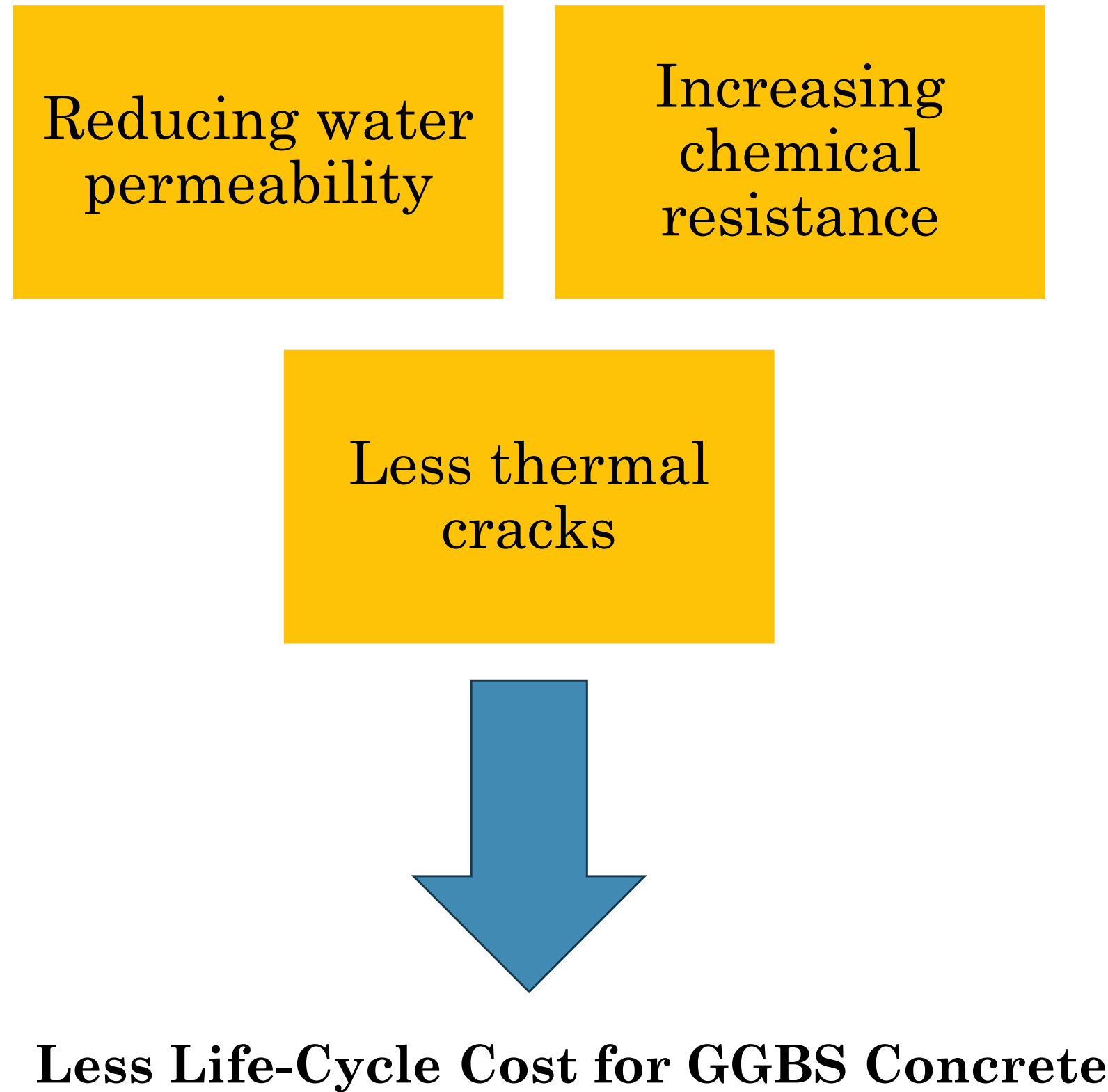
3. SUSTAINABLE CONSTRUCTION SOLUTIONS –

- ESG BENEFITS OF GGBS



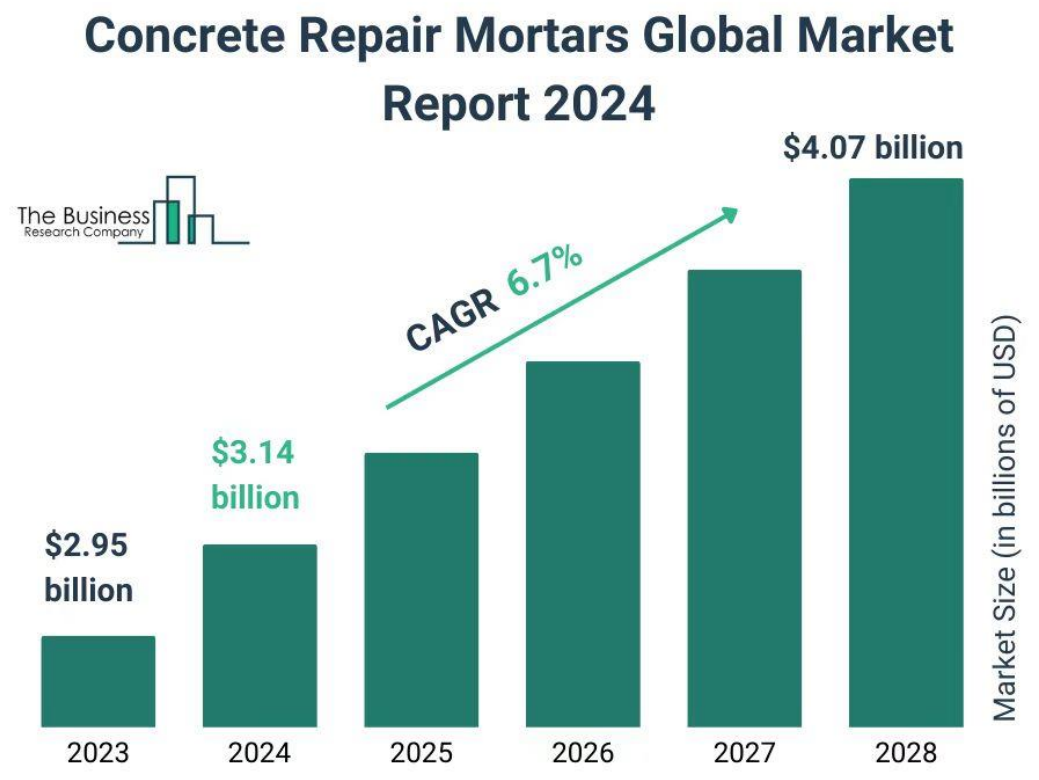
Benefits of GGBs Concrete in Environment

- Sustainability
- Recycling Materials Replacement
- Reducing Carbon Emission Factor



Enhance Concrete Durability

- Annual construction waste is expected to reach 2.2 billion tons globally by 2025

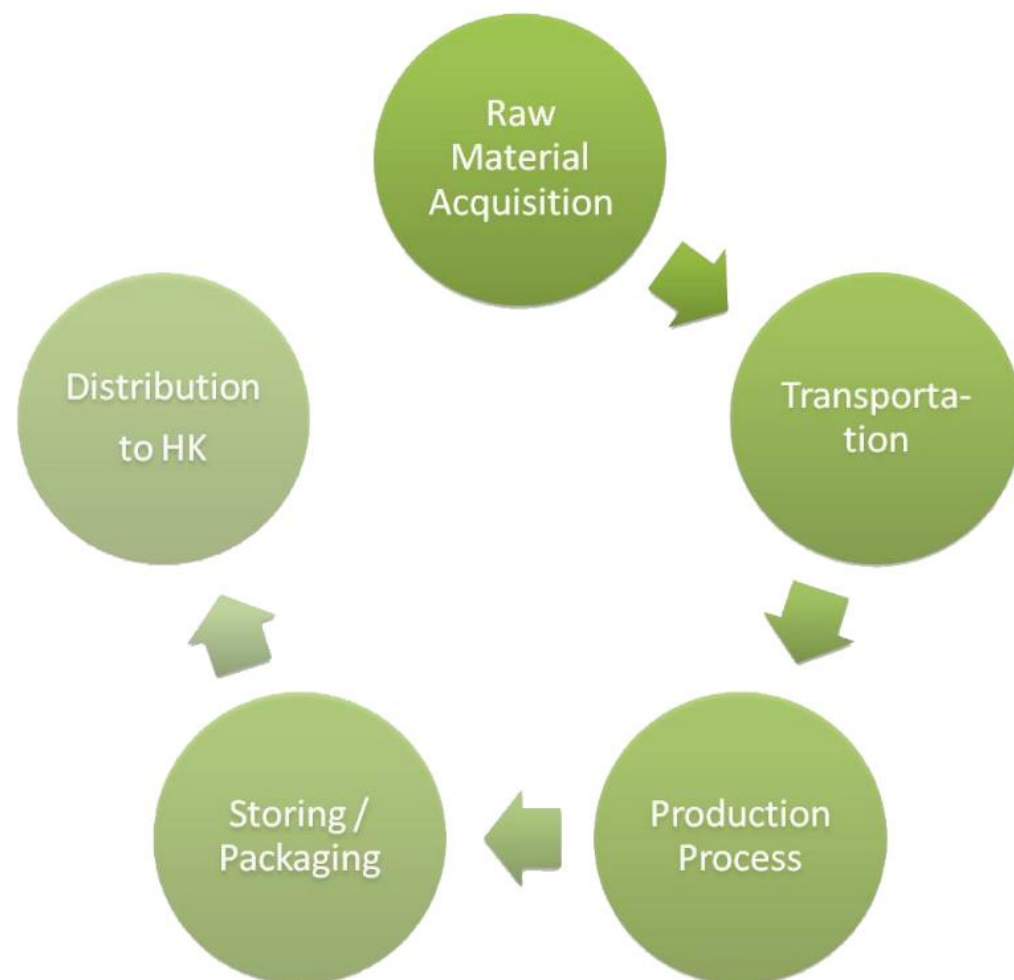


CIC Green Product Certification Introduction

Benchmark for Ready-mixed Concrete under the CIC Green Product Certification

ORIGINAL CIC Requirement:	C30		C35		C40		C45		C50		C60		C80	
	296		323		350		373		396		443		490	
Platinum	<	252	<	275	<	298	<	318	<	337		337		417
Gold	252	280	275	306	298	332	318	354	337	375	337	420	417	465
Silver	281	310	307	339	333	367	355	391	376	415	421	464	466	514
Bronze	311	340	340	372	368	403	392	429	416	455	465	509	515	563
Green	>	340	>	372	>	403	>	429	>	455		509		564

Carbon Assessment Method



- The quantification and reporting of the carbon footprint of products (CFP) under this Certification is thus based on a “cradle-to-site” approach, covering all GHG emissions and removals of the product arising from raw material acquisition to the border of Hong Kong.



Carbon footprint of Cementitious Materials

Cementitious Materials	Base Value in HK (kg CO ₂ /t)	Scope 1 – On-site emissions		Scope 2 – Power generation		Total (kg CO ₂ /t)
		Calcination of raw material	Fossil Fuel combustion	Clinker production	Grinding / Classification	
OPC	950	468	315	30	20	763
Classified PFA*	8		-		8	8
GGBS*	83		36		20	56

* Exclude the carbon emission in the primary process

碳係數名稱	生產區域名稱	數值	宣告單位	公告年份
卜特蘭水泥(II型)	臺灣	9.81E-1 kgCO ₂ e	公斤(kg)	2020
卜特蘭水泥(II型)	臺灣	9.64E-1 kgCO ₂ e	公斤(kg)	2019
鉍質水泥	歐洲	1.01E+1 kgCO ₂ e	公斤(kg)	2018
水泥熟料	臺灣	9.48E-1 kgCO ₂ e	公斤(kg)	2017
水泥(不分型號)	臺灣	9.07E-1 kgCO ₂ e	公斤(kg)	2017
水泥熟料	臺灣	9.50E-1 kgCO ₂ e	公斤(kg)	2014
卜特蘭水泥(乾式)	臺灣	9.40E-1 kgCO ₂ e	公斤(kg)	2014

Carbon emission of cement ~907kg/t

產品名稱	生產區域名稱	數值	宣告單位	公告年份
預拌混凝土(245 kgf/cm ²)	臺灣	2.52E+2 kgCO ₂ e	立方公尺(m ³)	2020
預拌混凝土(280 kgf/cm ²)	臺灣	3.38E+2 kgCO ₂ e	立方公尺(m ³)	2020
自充填預拌混凝土(350 kgf/cm ²)	臺灣	3.75E+2 kgCO ₂ e	立方公尺(m ³)	2020
預力梁用預拌混凝土(350 kgf/cm ²)	臺灣	4.07E+2 kgCO ₂ e	立方公尺(m ³)	2020
早強預拌混凝土(420 kgf/cm ²)	臺灣	3.70E+2 kgCO ₂ e	立方公尺(m ³)	2020
早強預拌混凝土(420kgf/cm ² · 飛灰矽石粉替代率22%)	臺灣	4.64E+2 kgCO ₂ e	立方公尺(m ³)	2019
早強預拌混凝土(420kgf/cm ² · 飛灰矽石粉替代率20%)	臺灣	4.31E+2 kgCO ₂ e	立方公尺(m ³)	2017
早強預拌混凝土(420kgf/cm ² · 飛灰矽石粉替代率25%)	臺灣	4.43E+2 kgCO ₂ e	立方公尺(m ³)	2017
早強預拌混凝土(420kgf/cm ² · 飛灰矽石粉替代率45%)	臺灣	3.36E+2 kgCO ₂ e	立方公尺(m ³)	2017
混凝土及水泥砂漿用大容高爐爐渣粉(散裝)	臺灣	5.04E+1 kgCO ₂ e	公噸(mt)	2016
混凝土及水泥砂漿用大容高爐爐渣粉(太空包裝)	臺灣	5.47E+1 kgCO ₂ e	公噸(mt)	2016
飛灰矽石粉(散裝)	臺灣	4.82E+1 kgCO ₂ e	公噸(mt)	2016
飛灰矽石粉(太空包裝)	臺灣	5.25E+1 kgCO ₂ e	公噸(mt)	2016

Carbon emission of GGBS ~50.4kg/t

Carbon emission factor for concrete mix

Normal Concrete						
	D45 OPC	D45 25% PFA	D45 45%GGBS	D60 OPC	D60 25% PFA	D60 45%GGBS
Cement	440	330	242	500	375	264
PFA	0	110	0	0	125	0
GGBS	0	0	198	0	0	216
Water	198	175	200	170	165	170
w/c	0.45	0.40	0.45	0.34	0.33	0.35
Carbon Emission Factor	367.651	281.605	226.188	415.542	317.123	244.564

Bored Pile				
	D45 25%PFA	D45 60%GGBS	D60 25% PFA	D60 60%GGBS
Cement	402	184	405	200
PFA	134	0	135	0
GGBS	0	276	0	300
Water	205	200	180	200
w/c	0.38	0.43	0.33	0.40
Carbon Emission Factor	337.219	192.514	339.978	207.446

Pile Cap				
	D40 35%PFA	D40 65%GGBS	D45 35%PFA	D45 65%GGBS
Cement	325	140	338	154
PFA	175	0	182	0
GGBS	0	260	0	286
Water	207	200	197	200
w/c	0.41	0.50	0.38	0.45
Carbon Emission Factor	276.7884	156.164	287.0238	169.548

Embodied carbon reduction in concrete:
 PFA concrete : ~25%
 GGBS concrete : 50%+

Lower Carbon Emission Factor

D45 OPC Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 327.673 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24096(RMC)
Licence End Date: 2027-11-18
Under new benchmark

D60 OPC Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 373.332 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24102(RMC)
Licence End Date: 2027-11-18
Under new benchmark

D45 PFA Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 261.561 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24097(RMC)
Licence End Date: 2027-11-18
Under new benchmark

D60 PFA Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 292.142 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24103(RMC)
Licence End Date: 2027-11-18
Under new benchmark

D45 GGBS Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 202.269 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24098(RMC)
Licence End Date: 2027-11-18

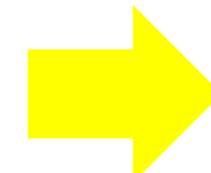
D60 GGBS Concrete

Manufacturer: Quon Hing Concrete Company Limited
Factory Site Address: TYTL 119, Tam Kon Shan Road, Tsing Yi, Hong Kong
Category: Ready-mixed concrete
Origin:
Carbon Rating:

CFP Value: 219.970 kg CO₂e/m³ product
Certificate No.: CICGPC-L-24104(RMC)
Licence End Date: 2027-11-18

ORIGINAL CIC Requirement:	C30	C35	C40	C45	C50	C60	C80
	296	323	350	373	396	443	490
Platinum	< 252	< 275	< 298	< 318	< 337	< 337	< 417
Gold	252	280	298	318	337	337	417
Silver	281	310	333	355	376	415	466
Bronze	311	340	368	392	416	455	515
Green	> 340	> 372	> 403	> 429	> 455	> 509	> 564

Proposed New Benchmarking	C30	C35	C40	C45	C50	C60	C80
	256	279	290	293	296	323	309
Platinum	< 218	< 238	< 247	< 250	< 252	< 246	< 263
Gold	218	242	247	250	252	246	263
Silver	243	268	276	279	281	281	294
Bronze	269	294	305	308	311	311	325
Green	> 294	> 321	> 334	> 337	> 340	> 340	> 356



Net-Zero emissions by 2035

Making it possible NOW

Thank
you...

Old History with New Horizon

through Innovation *for the next stage*



4. INNOVATIVE CONSTRUCTION METHODS - Ultrafine GGBS

This is the most update Low Carbon Cement and Concrete STANDARDS

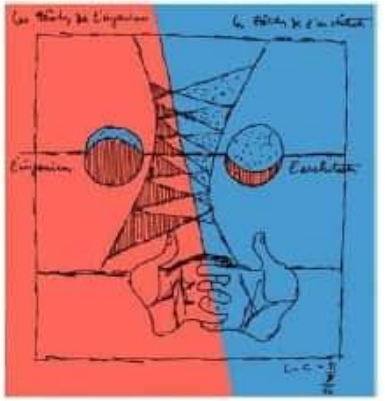
ACI CODE-323-24

Low-Carbon Concrete—
Code Requirements and
Commentary

Reported by ACI Committee 323

IN-LB Inch-Pound Units

Efficiency
Buildability
Quality

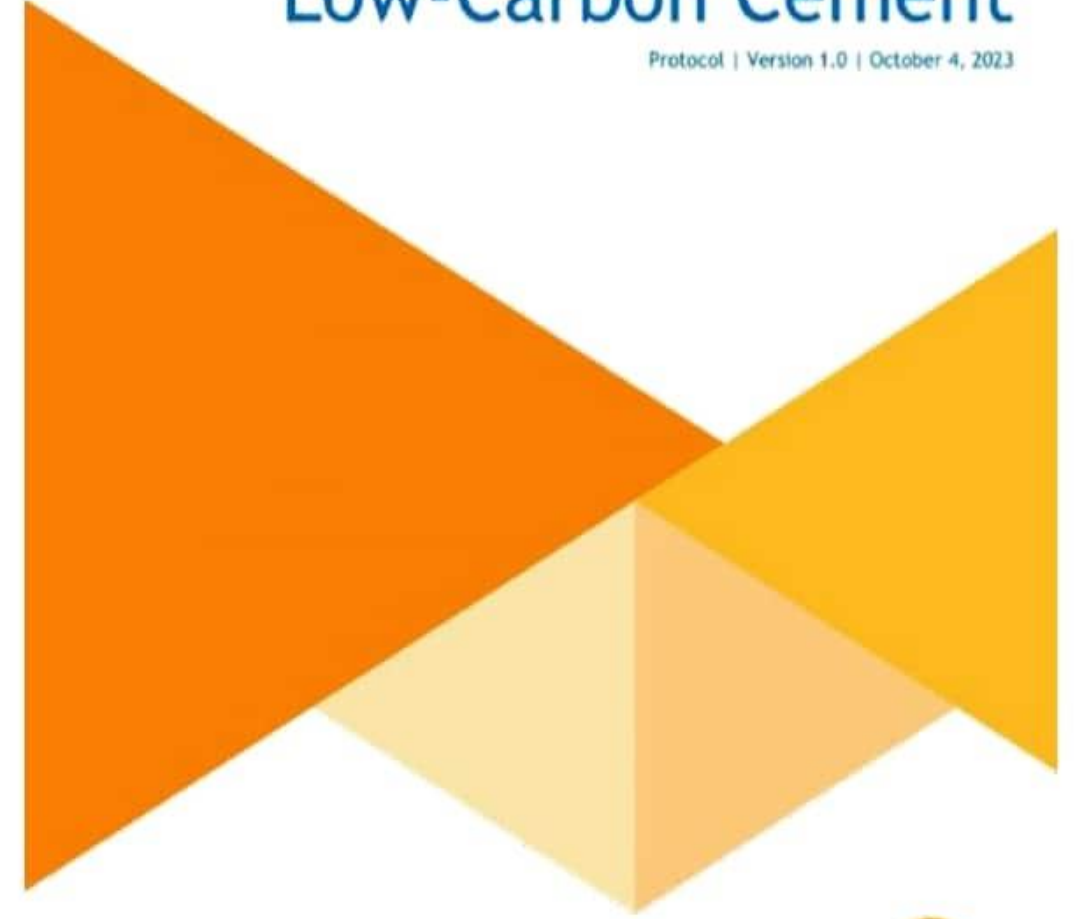


Rigidity
Strength/Load
Resilience

Material
Technologies



U.S.
Low-Carbon Cement
Protocol | Version 1.0 | October 4, 2023



.... to be able to face these new challenges ?



Getting The Balance Right.....

Independent Carbon Crediting Programmes – Low Carbon Cement Protocol

Additionality Requirement - Exceed Common Practice

Ineligible SCM/ACM List

- Portland Limestone Cement (ASTMC595)
- Traditional fresh coal ash (ASTM C618)
- Silica fume (ASTM C1240)
- Traditional Slag Cement (ASTM C595 & C989)
Grade 80 = (China S75)
Blaine- GGBS 3250cm²/g
Grade 100 = (China S95)
Blaine- GGBS 4100cm²/g
Grade 120 = (China S105)
Blaine- GGBS 5700cm²/g



ASTM - Slag Activity Index, min, %		
Average of Consecutive	Last Five Samples	Individual Sample
7-Day Index		
Grade 100	75	70
Grade 120	95	90
28-Day Index		
Grade 100	95	90
Grade 120	115	110

Eligible Products

Examples of eligible SCMs/ACMs include:

- Beneficiated coal ash (upgraded and/or harvested coal or bottom ash)
- Raw natural pozzolans (i.e., volcanic ash)
- Calcined clays/shale and/or metakaolin
- Limestone calcined clay cements (LC3)
- Carbon dioxide (CO₂)
- Other artificial pozzolans or treated calcined materials (including rice husk ash)
- Other waste by-products (including Bauxite residue (Red Mud) or cement kiln dust)
- Novel ACMs (including clinkered, calcined, and non-clinkered materials)
- Hydroxide products (including portlandite (Ca(OH)₂) and brucite (Mg(OH)₂))
- **Other novel SCM/ACM s (including biogenic limestone, etc)**
- Blends including one or more eligible SCMs/ACMs

Project Developers

The project developer by default is the SCM/ACM supplier or manufacturer, but a project developer may also be low-carbon cement technology suppliers, and/or entities that specialize in project development.



China and India High Fineness GGBS Standard

本标准主要起草人:高春勇、姚燕、王玲、王军伟、李建勇、沈平邦、赵磊、孙继成、李培彦、王斌、高博、

ICS 91.100.30
Q 13



高强高性能混凝土用矿物外加剂

Mineral admixtures for high strength
and high performance concrete

中华人民共和国国家标准

表 1 矿物外加剂的技术要求
GGBS Fineness

GB/T 18736—2017
代替 GB/T 18736—2002
2017 Version

试验项目	磨细矿渣		粉煤灰	磨细天然沸石	硅灰	偏高岭土	
	I	II					
氧化镁(质量分数)/%	≤ 14.0		—	—	—	4.0	
三氧化硫(质量分数)/%	≤ 4.0		3.0	—	—	1.0	
烧失量(质量分数)/%	≤ 3.0		5.0	—	6.0	4.0	
氯离子(质量分数)/%	≤ 0.06		0.06	0.06	0.10	0.06	
二氧化硅(质量分数)/%	—	—	—	—	85	50	
三氧化二铝(质量分数)/%	—	—	—	—	—	35	
游离氧化钙(质量分数)/%	—	—	1.0	—	—	1.0	
吸铵值/(mmol/kg)	—	—	—	1 000	—	—	
含水率(质量分数)/%	≤ 1.0		1.0	—	3.0	1.0	
细度	比表面积/(m ² /kg)	≥ 600	400	—	—	15 000	—
	45 μm 方孔筛筛余(质量分数)/%	≤ —	—	25.0	5.0	5.0	5.0
需水量比/%	≤ 115	105	100	115	125	120	
活性指数/%	3 d	80	—	—	90	85	
	7 d	100	75	—	95	90	
	28 d	110	100	70	95	105	

Table 4. Chemical characteristics of ultrafine GGBS

S. No.	Chemical component	Value (% by mass)
1	Manganese oxide (MnO)	0.45
2	Magnesium oxide (MgO)	8.91
3	Sulphide sulphur (S)	0.63
4	Sulphate (SO ₄ ²⁻)	0.22
5	Chloride content (Cl ⁻)	0.07
6	CaO	33.03
7	SiO ₂	33.80
8	Glass content	93.50

Table 5. Physical characteristics of GGBS

Characteristic	Value
Particle size (μm)	
D50	3.90
D95	14.21
Fineness (m²/kg)	1822
Slag activity index %	
7 days	94.6
28 days	114
Specific gravity	2.82

GGBS Fineness And Replacement Ratio Effect On Concrete Compressive Strength

Korea Study

ID	Setting time(min)	
	Initial	Final
Plain	255	321
HV35B1	366	455
HV35B2	371	458
HV35B3	390	491
HV35B4	396	470
HV50B1	435	556
HV50B2	414	541
HV50B3	415	530
HV50B4	442	560
HV65B1	330	645
HV65B2	375	652
HV65B3	345	825
HV65B4	581	748
HV80B1	205	1105
HV80B2	255	1105
HV80B3	365	1140
HV80B4	385	735

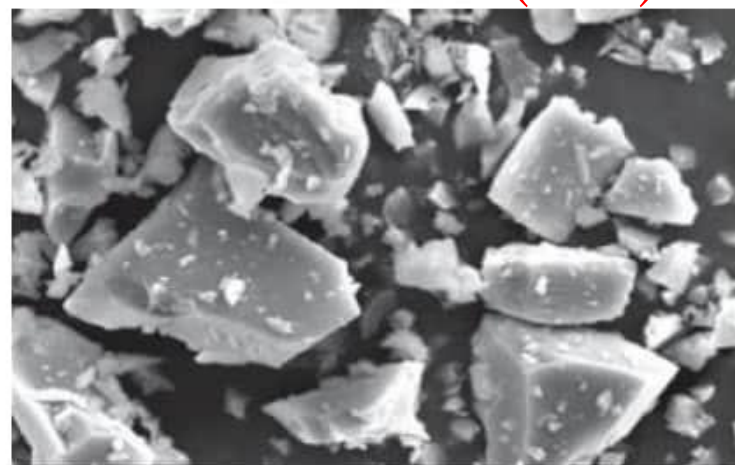
ID		Unit weight(kg)					
		water	OPC	GB1	GB2	GB3	GB4
0%	Plain	2.4	12.0	-	-	-	-
	HV35B1	2.4	7.8	4.2	-	-	-
35%	HV35B2	2.4	7.8	-	4.2	-	-
	HV35B3	2.4	7.8	-	-	4.2	-
	HV35B4	2.4	7.8	-	-	-	4.2
	HV50B1	2.4	6	6	-	-	-
50%	HV50B2	2.4	6	-	6	-	-
	HV50B3	2.4	6	-	-	6	-
	HV50B4	2.4	6	-	-	-	6
	HV65B1	2.4	4.2	7.8	-	-	-
65%	HV65B2	2.4	4.2	-	7.8	-	-
	HV65B3	2.4	4.2	-	-	7.8	-
	HV65B4	2.4	4.2	-	-	-	7.8
	HV80B1	2.4	2.4	9.6	-	-	-
80%	HV80B2	2.4	2.4	-	9.6	-	-
	HV80B3	2.4	2.4	-	-	9.6	-
	HV80B4	2.4	2.4	-	-	-	9.6

GGBS Fineness and Replacement Ratio On Concrete Compressive Strength At Water/Binder Ratio = 0.24							
Blaine B1=4,350 cm ² /g, Blaine B2=5,350 cm ² /g, Blaine B3=6,450 cm ² /g, Blaine B4=7,650 cm ² /g,							
GGBS Replacement	ID	Flow (mm)	Compressive Strength (MPa)				
			3 day	7 day	28 day	91 day	
35%	Blaine B1~B4	Plain	202.0	82.0	91.9	107.3	131.3
		HV 35 B1	415.0	87.2	104.2	136.7	152.5
		HV 35 B2	411.5	90.5	110.7	141.2	151.5
		HV 35 B3	405.5	88.1	113.4	136.5	153.9
50%	Blaine B1~B4	HV 35 B4	363.0	95.4	111.2	142.5	154.7
		HV 50 B1	424.5	78.3	111.9	142.5	157.2
		HV 50 B2	425.0	86.6	112.6	145.8	158.3
		HV 50 B3	410.0	90.7	114.6	144.2	156.1
65%	Blaine B1~B4	HV 50 B4	366.0	92.7	112.0	123.7	154.5
		HV 65 B1	458.5	75.3	126.0	142.2	163.7
		HV 65 B2	442.0	80.2	119.8	128.0	155.0
		HV 65 B3	436.0	78.5	117.5	128.0	142.6
80%	Blaine B1~B4	HV 65 B4	407.0	82.8	118.4	131.9	149.0
		HV 80 B1	441.5	60.7	109.4	118.1	125.7
		HV 80 B2	448.0	68.1	114.7	121.5	138.2
		HV 80 B3	453.5	70.3	117.9	119.3	136.2
	Blaine B1~B4	HV 80 B4	412.0	78.6	97.7	113.1	121.0

Japan GGBS Slag Activity Index And Blaine Fineness

各種高炉スラグ微粉末の SEM 画像

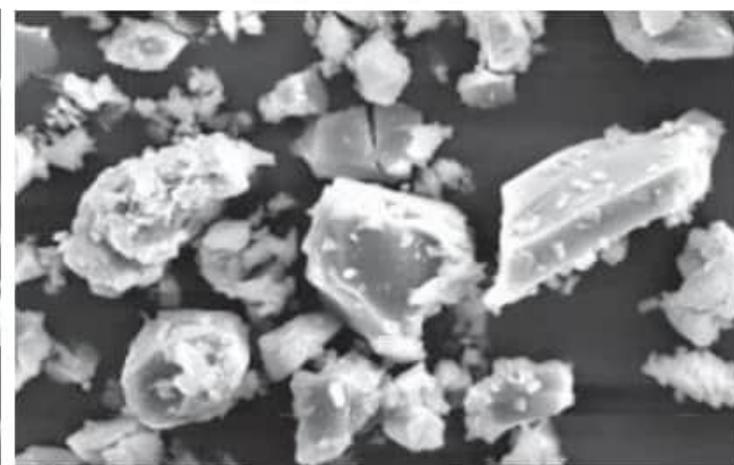
BF4000 (S95)



1000 倍

5μm

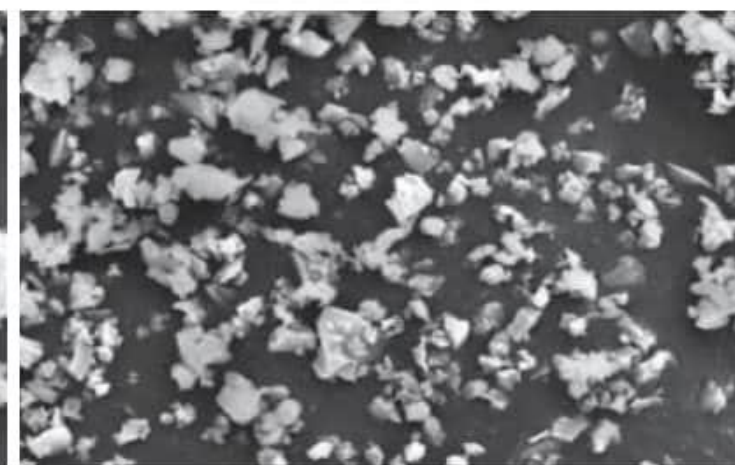
BF8000



1000 倍

5μm

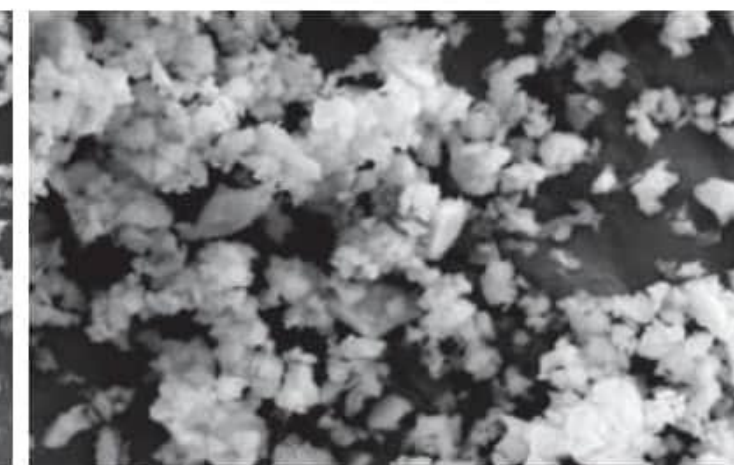
BF11000



1000 倍

5μm

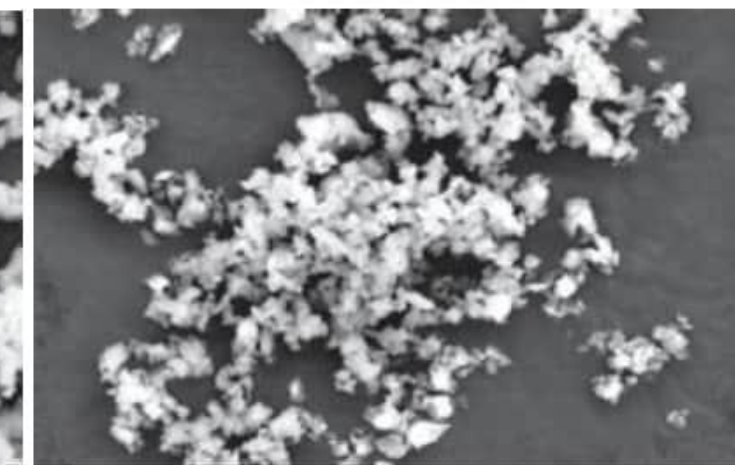
BF18000



1000 倍

5μm

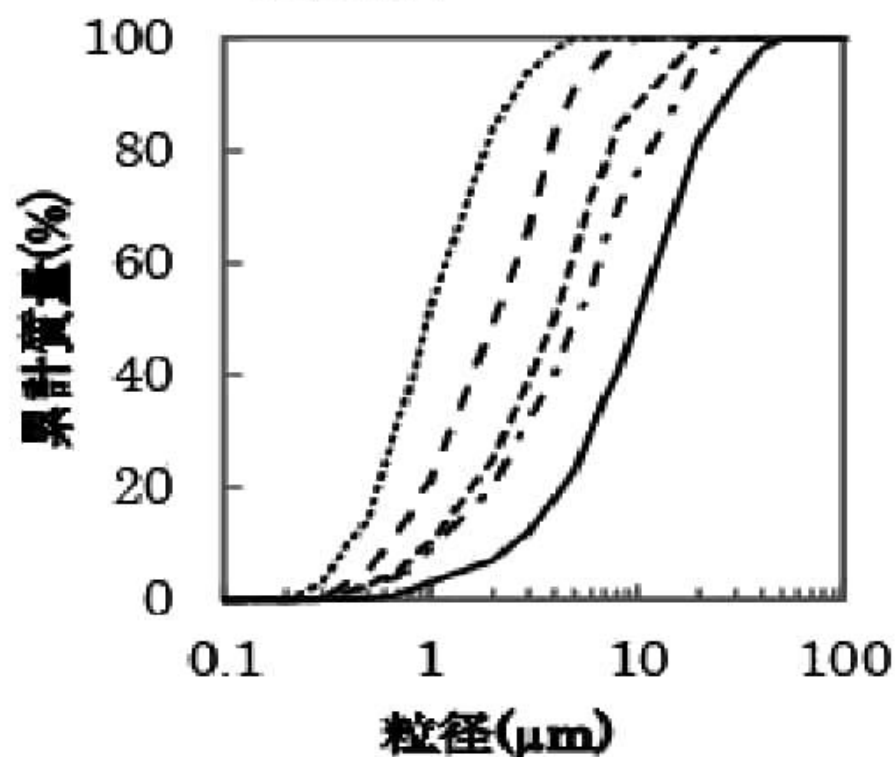
BF30000



1000 倍

5μm

——— BF4000 - - - - - BF8000
 - - - - - BF11000 - - - - - BF18000
 ······· BF30000



高炉スラグ微粉末の種類および物性

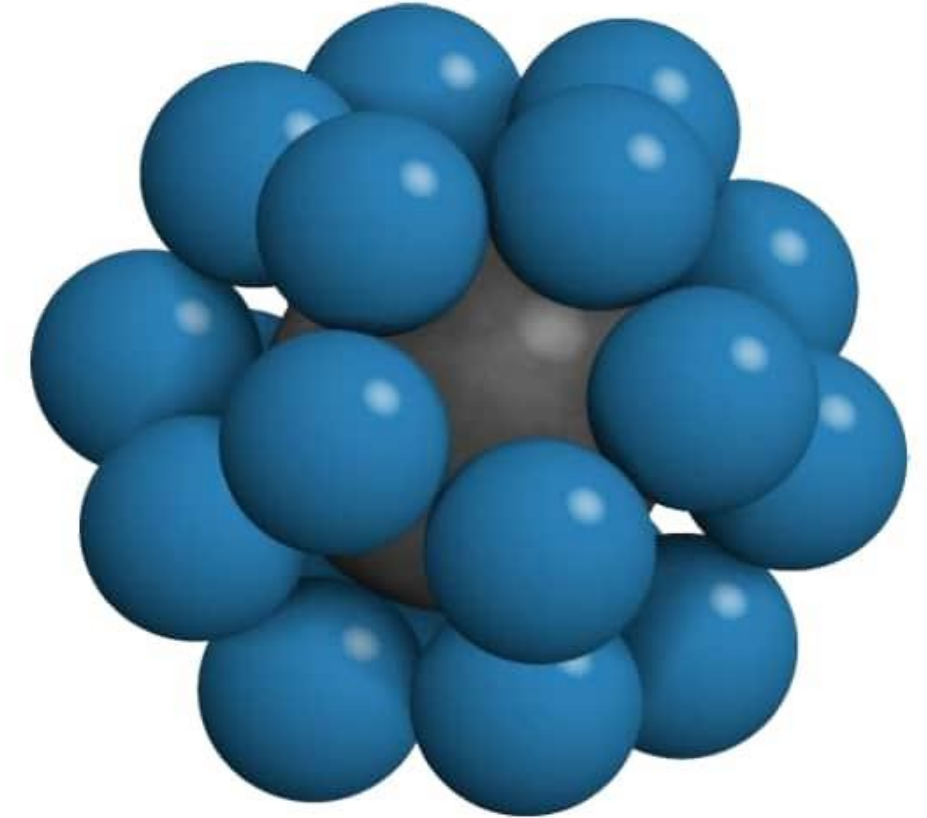
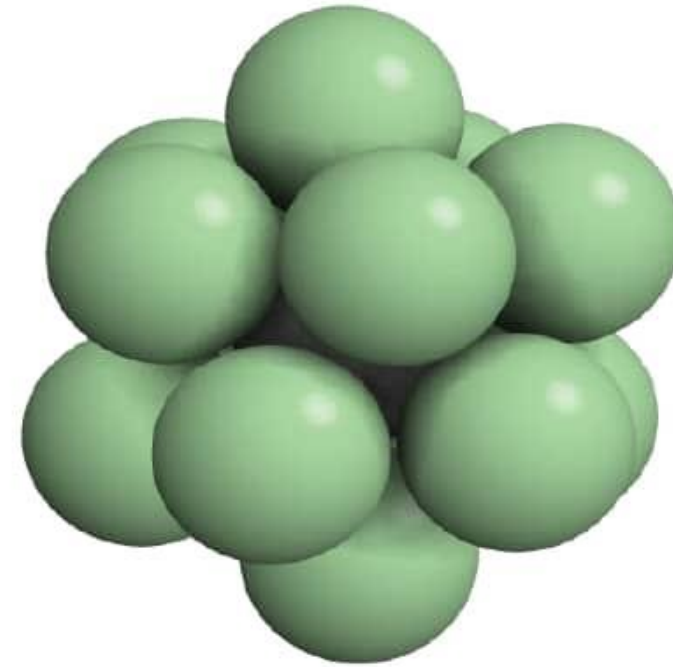
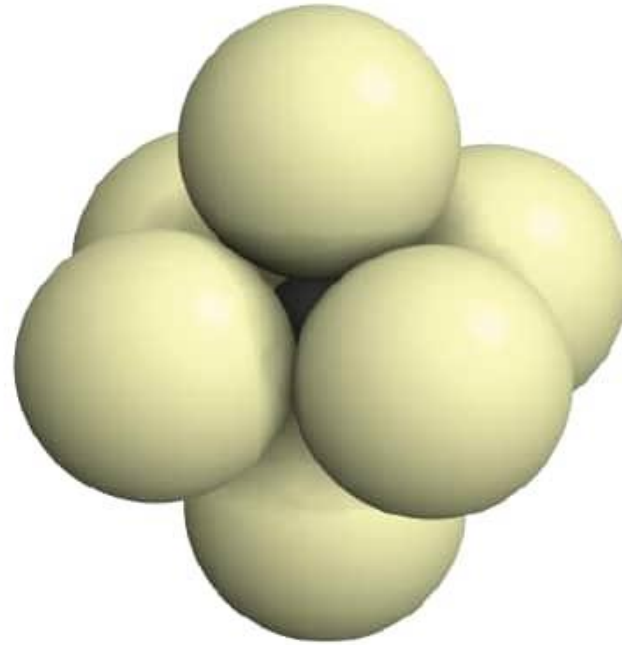
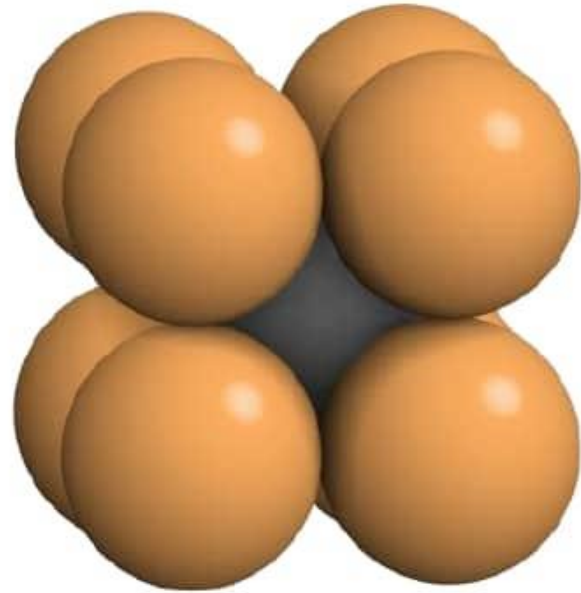
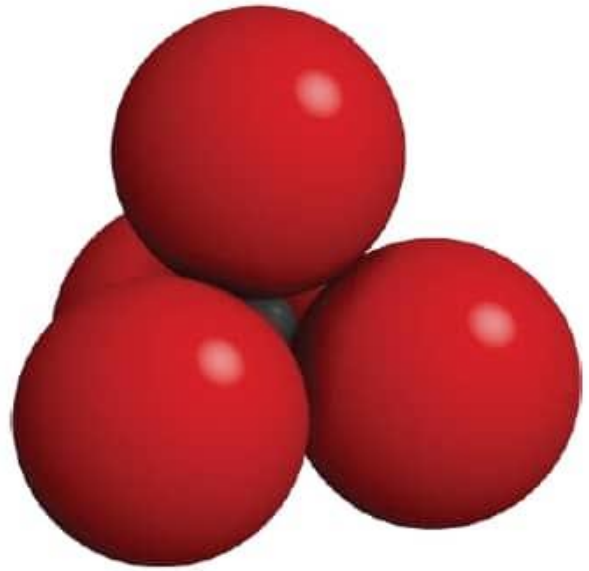
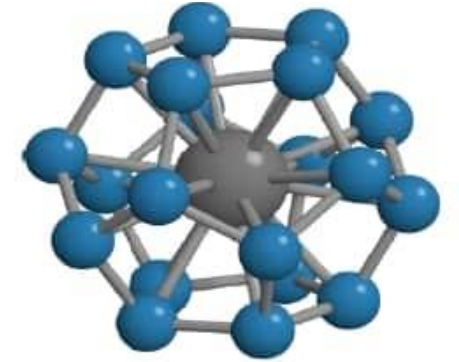
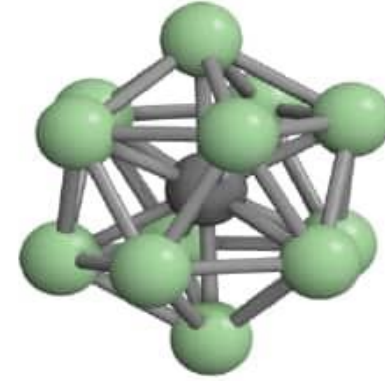
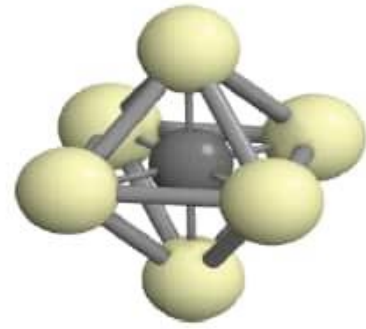
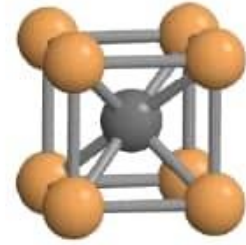
Production Using Air Classifier	種類					
	BF4000	BF8000	BF11000	BF18000	BF30000	
密度(g/cm ³)	2.92	2.92	2.92	2.92	2.92	
比表面積(cm ² /g)	4830	8180	10800	18050	29620	
平均粒径(μm)	9.6	5.2	4.0	2.0	1.0	
ブロー値比(%)	100	99	98	93	86	
活性度 指数 (%)	7 日	67	98	100	154	164
	28 日	99	112	128	138	138
	91 日	105	120	122	118	111

高炉スラグ微粉末の
化学成分

化学成分 (%)	試験値	JIS A 6206 の規定値
ig.loss	0.55	3.0 以下
insol	0.64	—
SiO ₂	32.7	—
Al ₂ O ₃	13.4	—
Fe ₂ O ₃	0.5	—
CaO	41.6	—
Na ₂ O	0.22	—
K ₂ O	0.28	—
MgO	6.9	10 以下
SO ₃	0.34	4.0 以下
Cl ⁻	0.0003	0.02 以下

NEXT Expanding Cement Paste Property Space

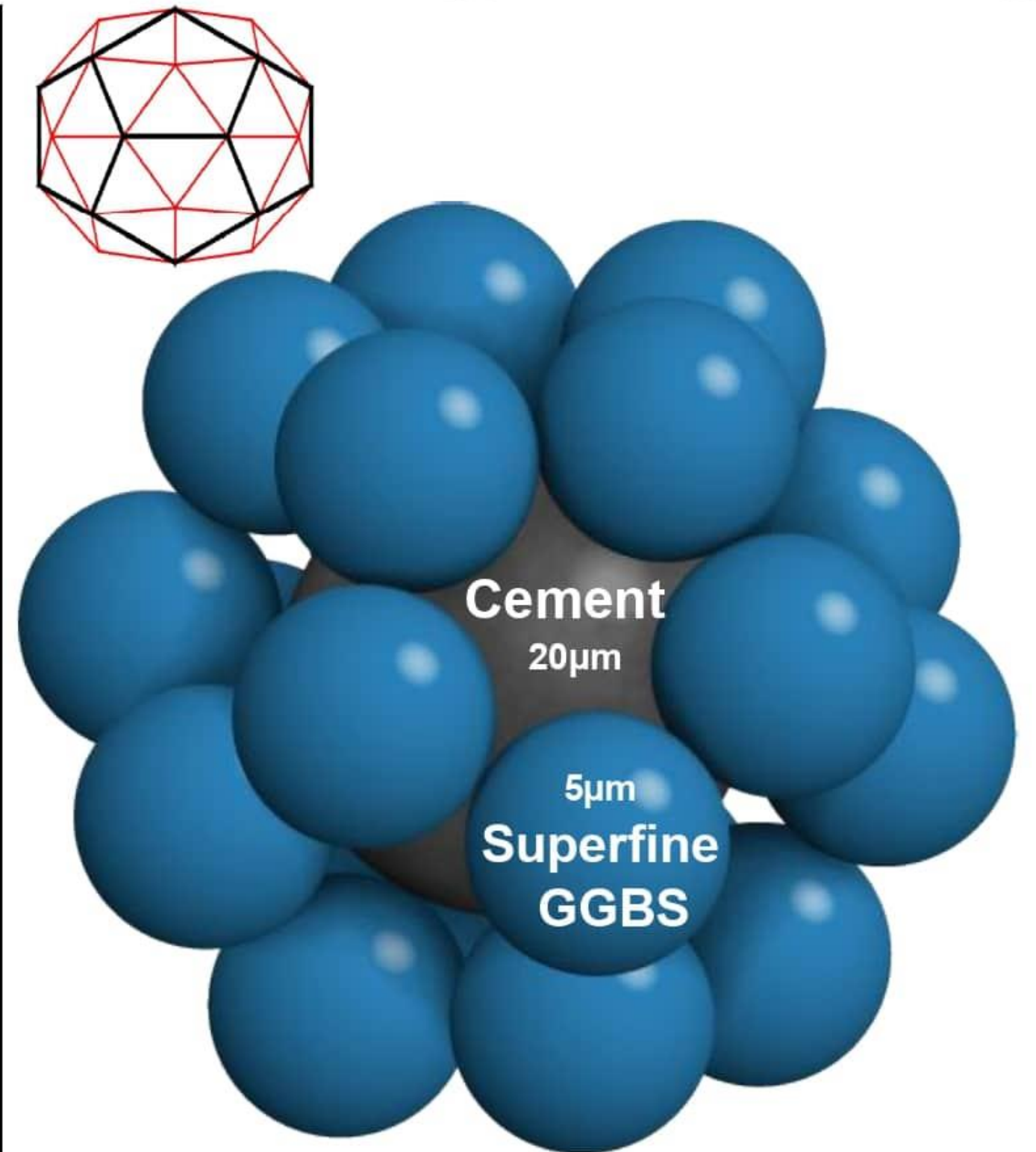
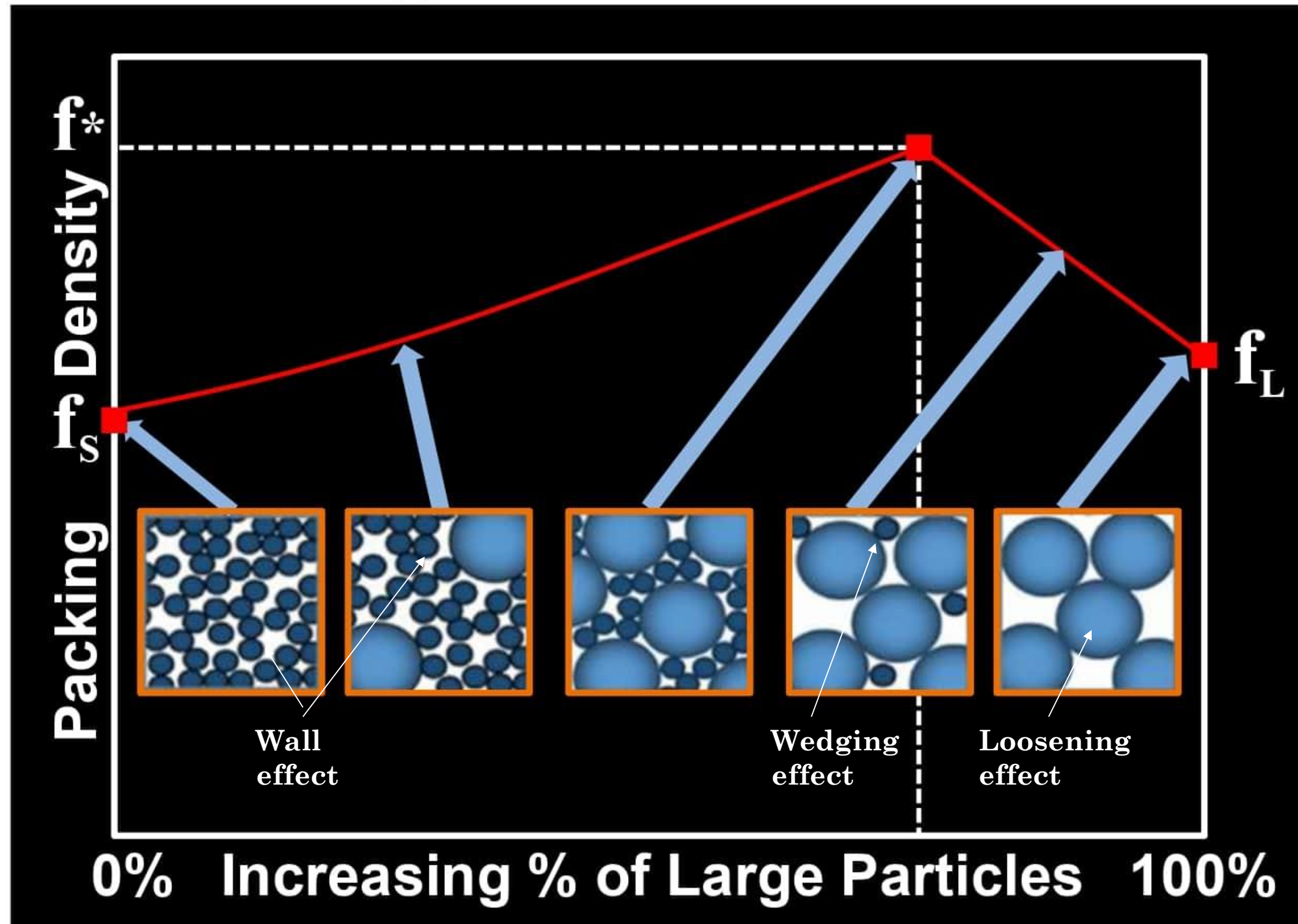
Concept of Packing Density



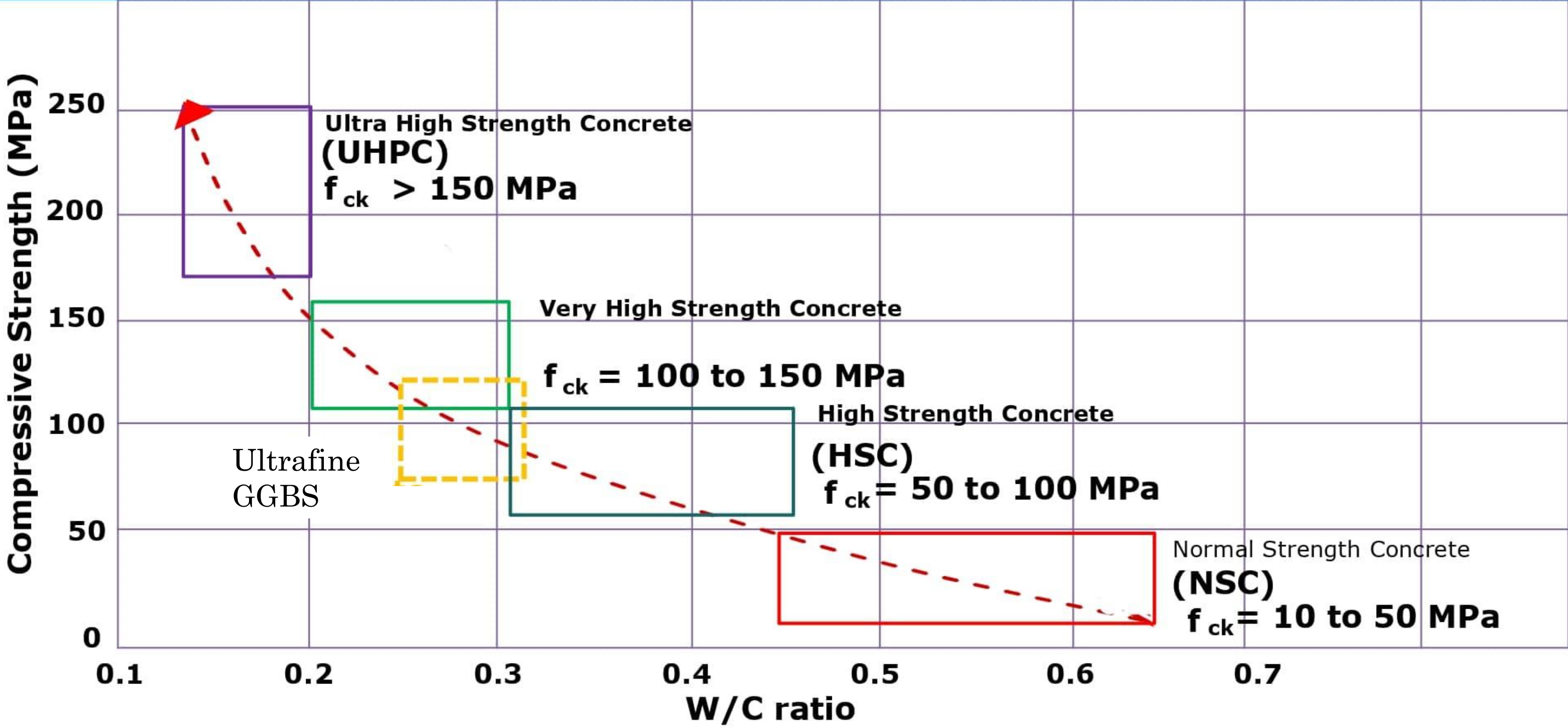
Filler Effect

Occupying Effect

Tailoring Bimodal Local Packing Density

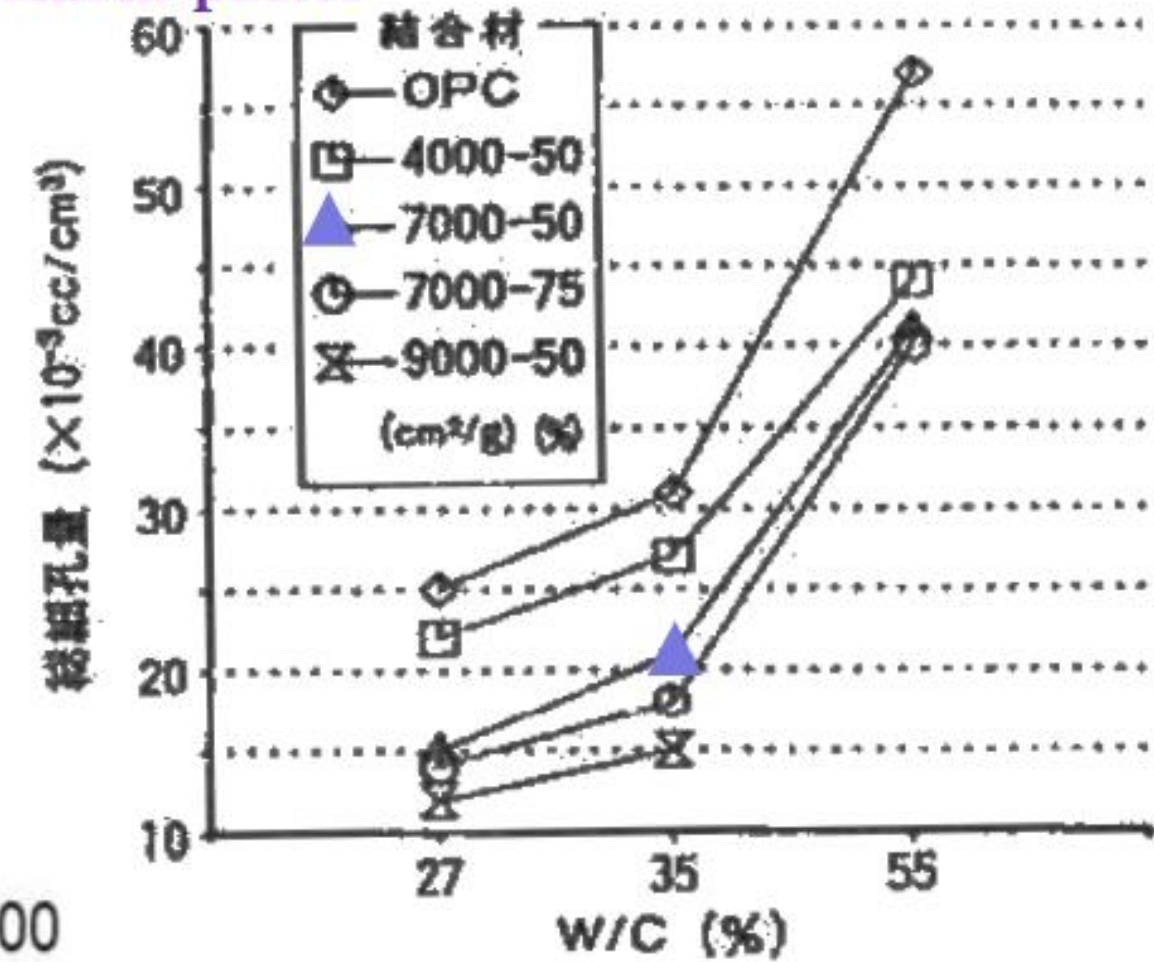
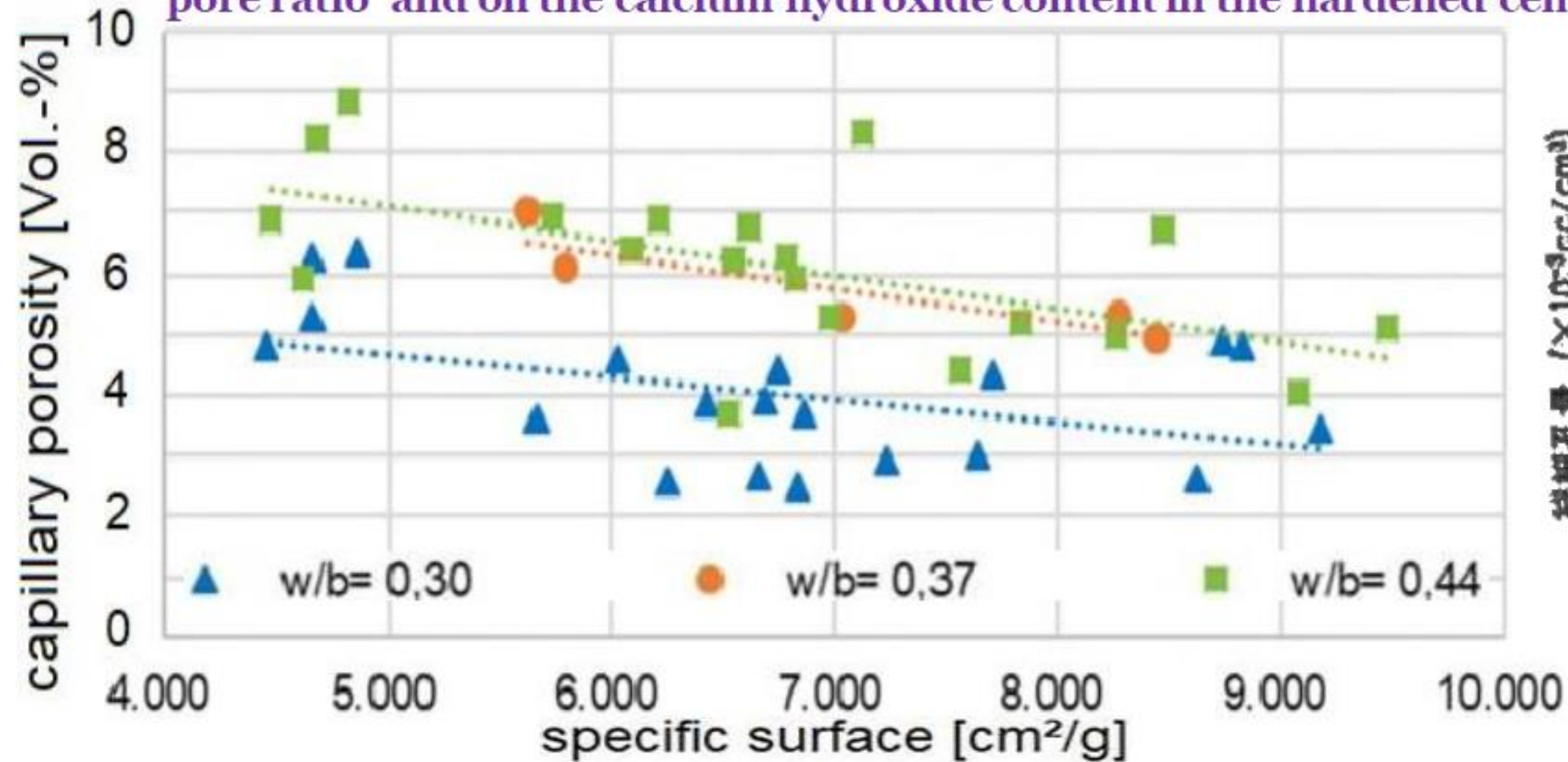


CONCRETE PERFORMANCE push continuously upwards



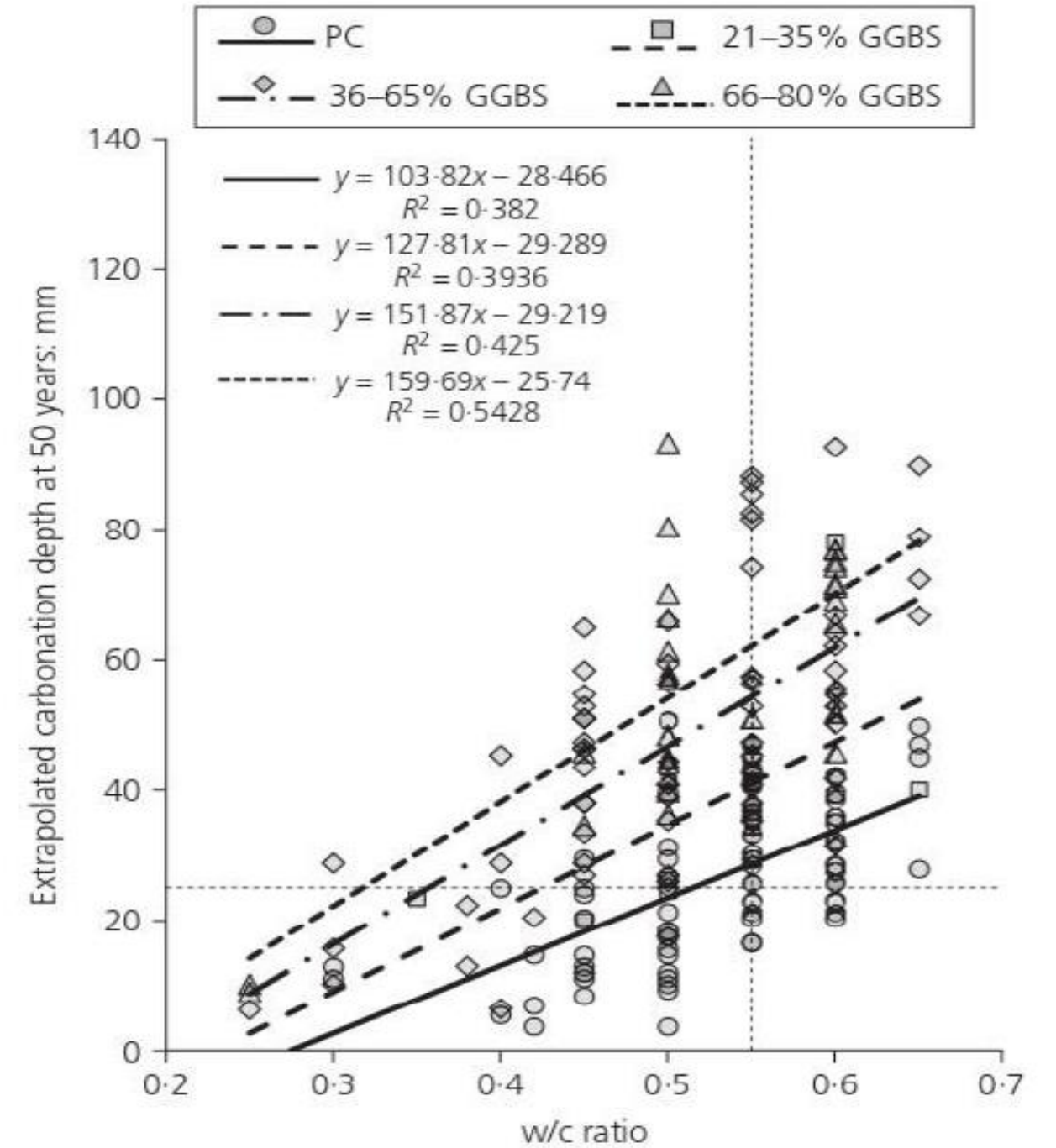
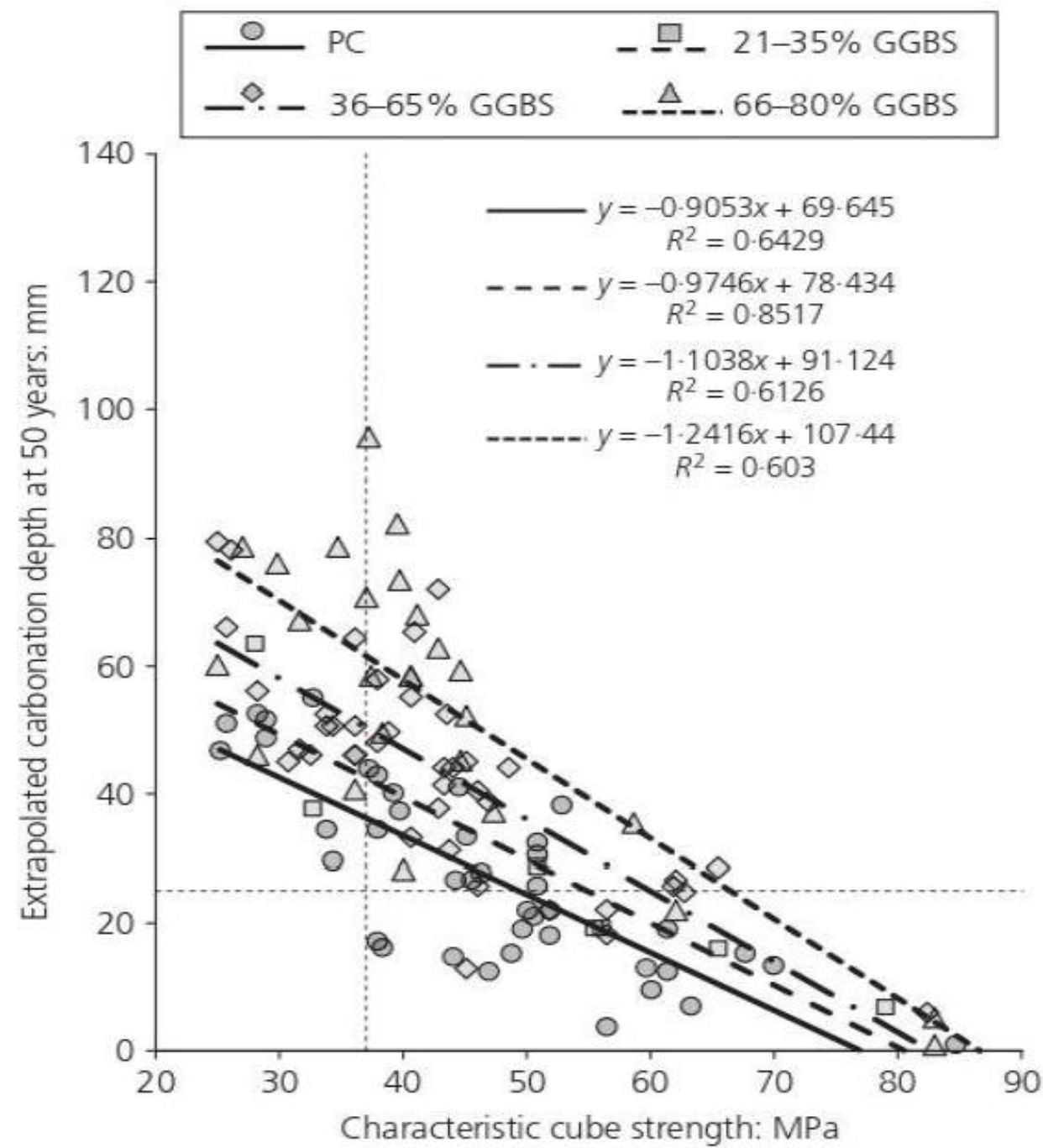
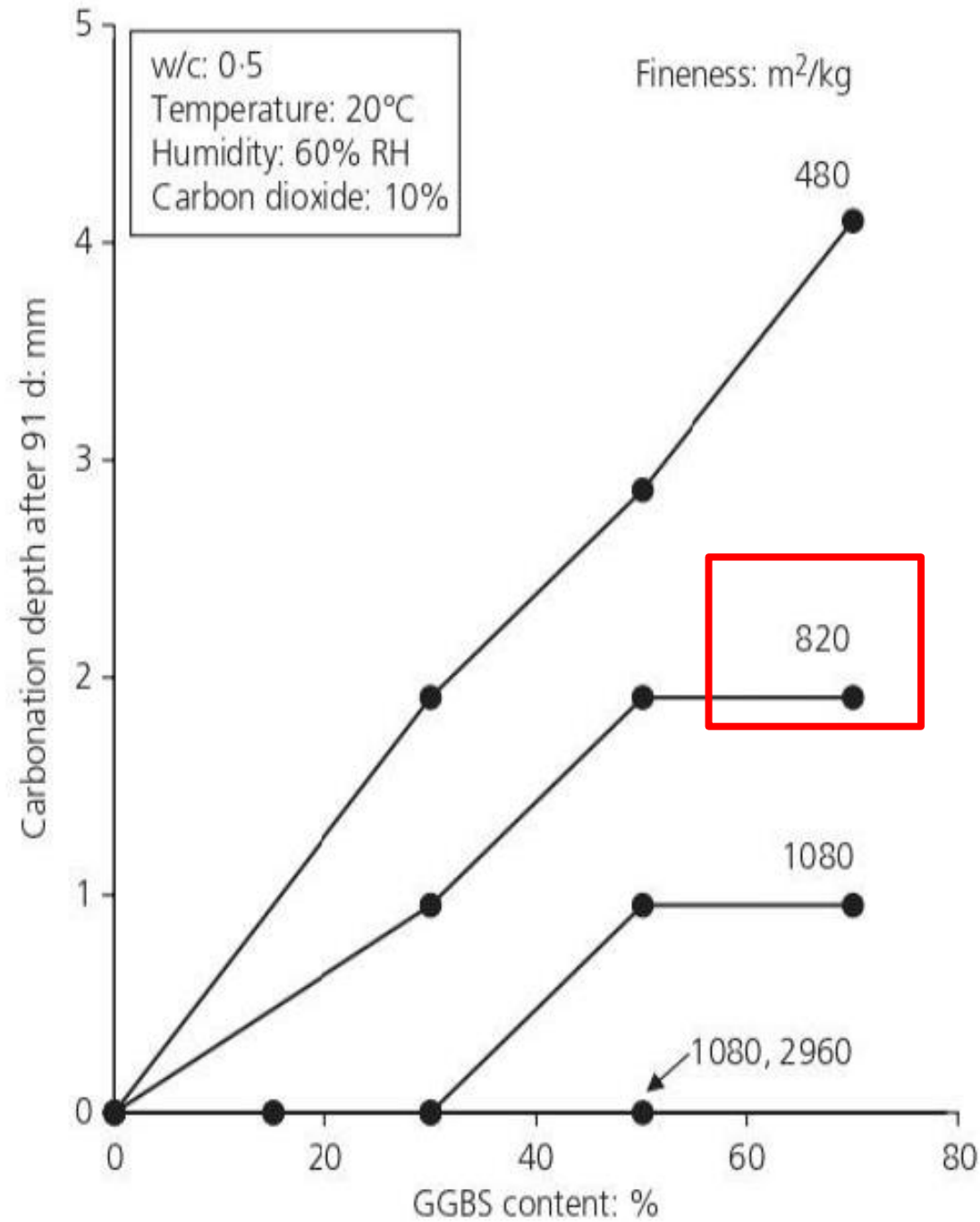
2. High Fineness GGBS Capillary Pore Size

High (ultra-fine) granulated blast furnace slag content has a favourable effect both on the capillary/gel pore ratio and on the calcium hydroxide content in the hardened cement paste.



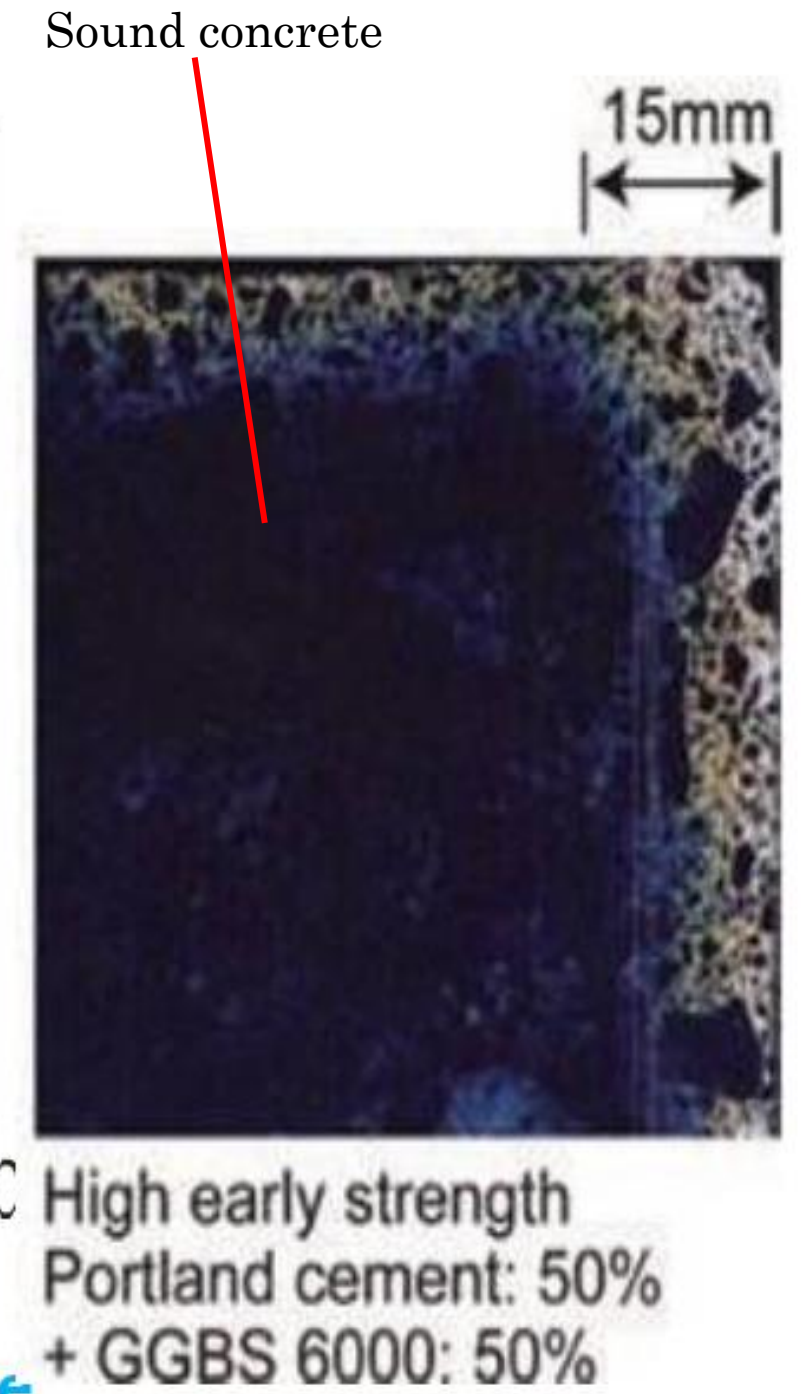
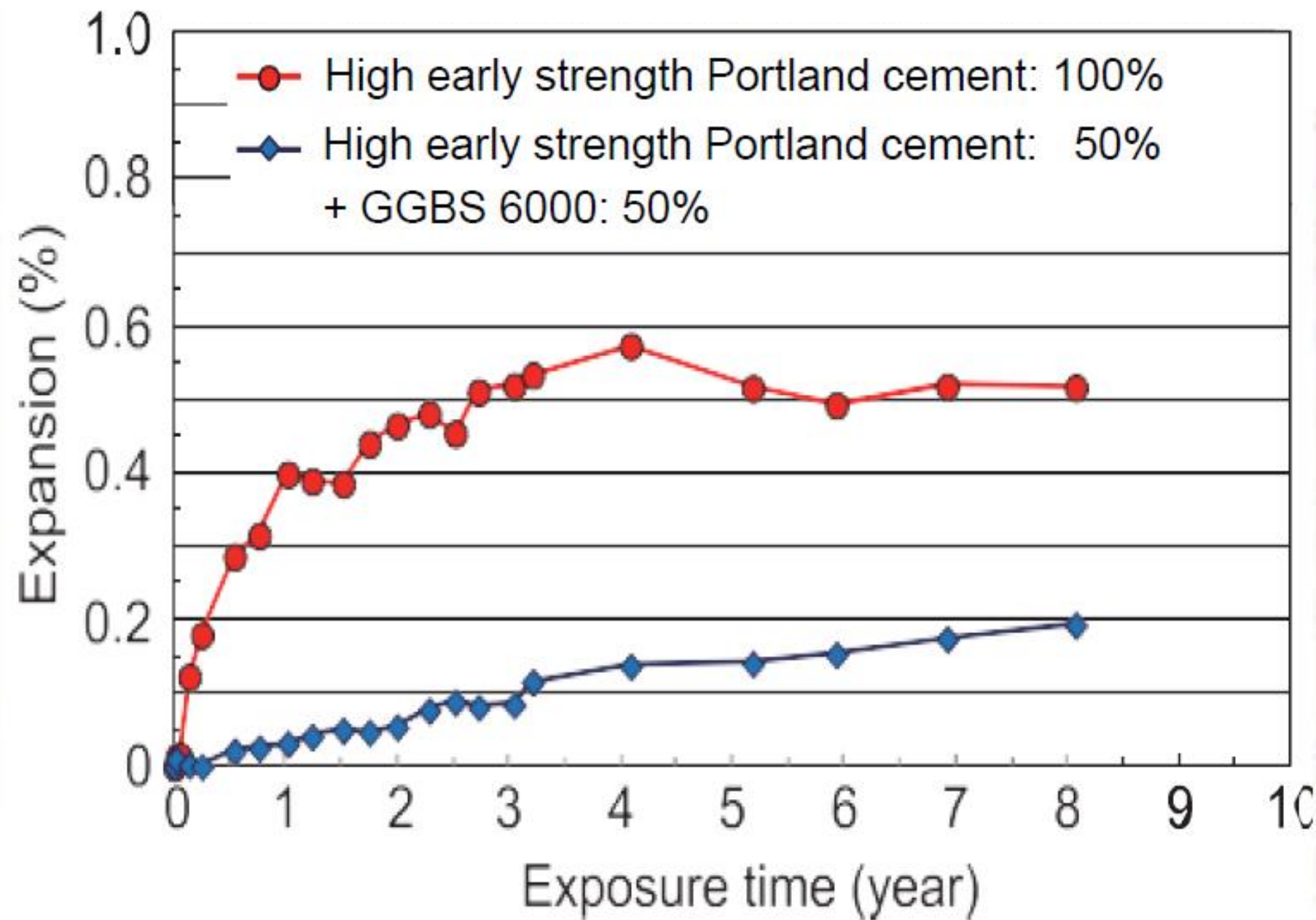
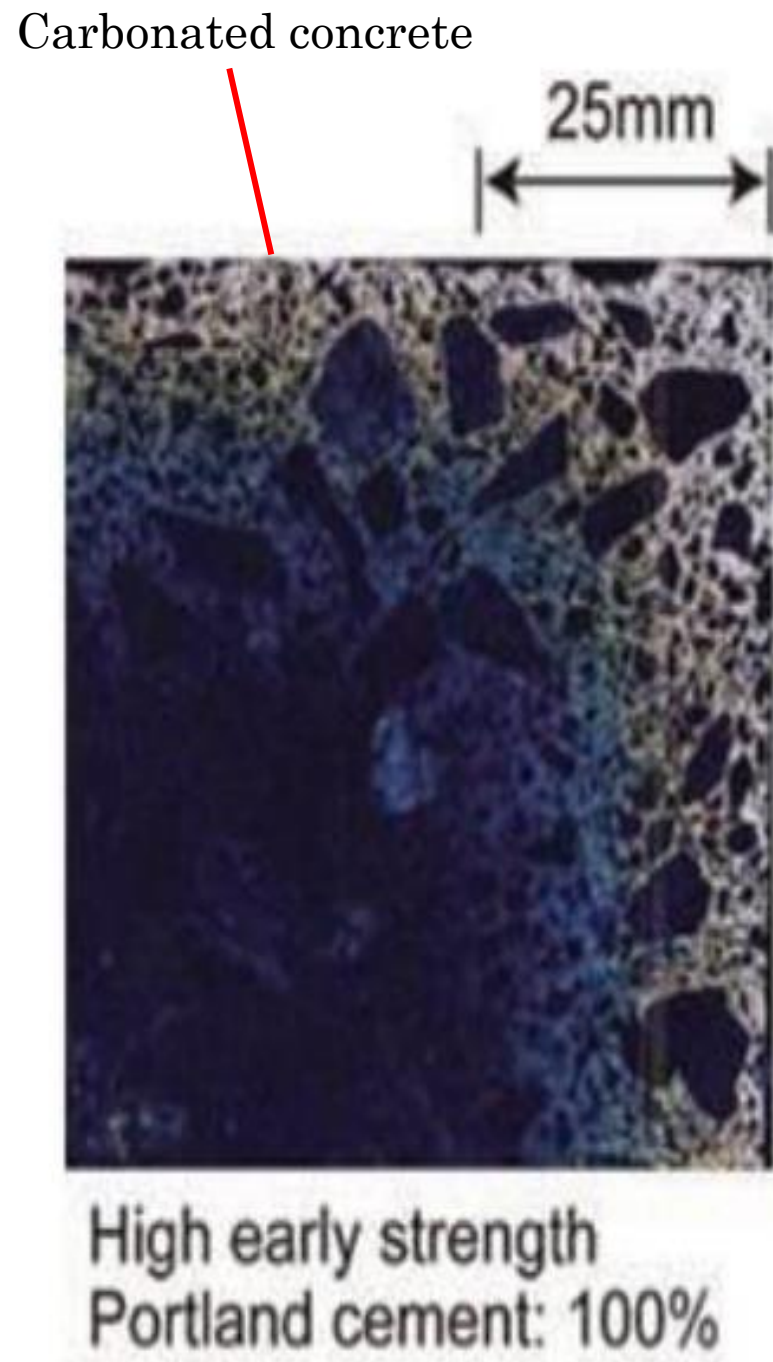
Impact of w/b ratio and specific surface on the capillary porosity

3. High Fineness GGBS Carbonation Resistance



Slag %, Slag Fineness, Compressive Strength and W/B ratio on Carbonation Depth

4. High Fineness GGBS ASR Resistance



ASR expansion of PC beam made with reactive aggregate

Superfine GGBS Fineness and Substitution Rate On Concrete Properties

	Type	S 95 GGBS 4000			Ground granulated blast-furnace slag 6000		
		3000	≧	< 5000	5000	≧	< 7000
		35	50	70	35	50	70
Property of fresh concrete	Blaine specific surface area (cm ² /g)						
	Substitution ratio (%)						
	Fluidity	○	○	○	◎	◎	◎
	Bleeding	○	○	△	◎	◎	◎
	Setting delay effect	◎	◎	◎	◎	◎	◎
Property of strength	Adiabatic temperature rise	–	–	◎	–	–	◎
	Heat generation rate restraint	○	◎	◎	○	○	◎
	Initial strength	○	△	△	○	○	△
	28 days strength	○	○	△	○	◎	◎
	Long-term strength	○	◎	◎	○	◎	◎
Property of durability	High strength	○	△	△	○	◎	◎
	Drying shrinkage	○	○	○	○	○	○
	Carbonation	–	–	△	–	–	△
	Freeze thaw	○	○	○	○	○	○
	Water-tightness	○	◎	◎	○	◎	◎
	Salt shield	○	◎	◎	○	◎	◎
	Seawater resistant	○	◎	◎	○	◎	◎
	Acid and sulfates resistant	○	◎	◎	○	◎	◎
	Heat resistant	○	○	○	○	○	○
	Alkali-silica restraint	○	◎	◎	○	◎	◎
Abrasion resistance	○	○	○	○	○	◎	

Legend: ◎ : Good property is provided in comparison with no mixture concrete. △ : Attention is necessary for use.
 ○ : At the same level or a little good property is provided. – : Property varies according to a condition.

G.Seed IP Protected Innovation

Intellectual Property Assets

PCT PATENT NO :
WO2024065340

PCT PATENT NO :
WO2023082040

G.Seed
Products



G.S.T
G.Seed Binder

G.S.T
Novel Rebar

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International Bureau

(43) International Publication Date
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(10) International Publication Number
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PCT/CN2022/122356
- (22) International Filing Date:
29 September 2021 (29.09.2021)
- (25) Filing Language:
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- (71) Applicant: **FLEXCRETE TECHNOLOGY LIMITED**
[CN/CN]; Unit 6, 15/F., Tower 1, Ever Gain Plaza, 88 Container Port Road, Kwai Chung, New Territories, Hong Kong (CN).
- (74) Agent: **RUNPING & PARTNERS**; Suite 515, Yingu Mansion, No.9 Beishuansilu, Haidian District, Beijing 100190 (CN).
- (81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CV, CZ, DE, DJ, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IQ, IR, IS, IT, JM, JO, JP, KE, KG, KH, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, WS, ZA, ZM, ZW.
- Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SC, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

(54) Title: HARMONIC-STRUCTURED HYDRAULIC BINDER, MANUFACTURING METHOD THEREOF AND STRENGTH-DECOUPLED HIGH ELASTIC MODULUS CEMENTITIOUS COMPOSITE MATERIAL MADE USING THE SAME.

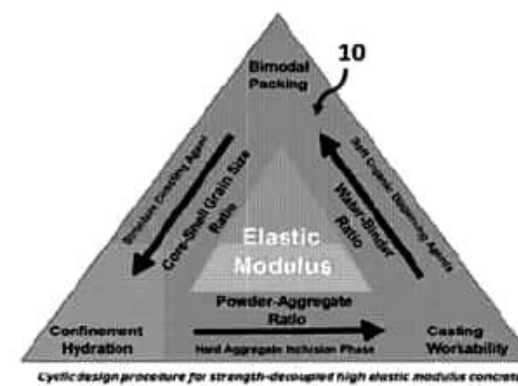


FIG. 7c

(57) Abstract: A novel strength-decoupled high elastic modulus cementitious composite (10), and a novel harmonic-structured hydraulic binder compositions (11). The compositions (11) comprise an effective amount of bimodal coarse (21) and ultrafine hydraulic particles (27) forming core-shell self-assembled clusters matrix. The cementitious composite (10) elements show substantial improved elastic modulus and durability material properties, particularly towards structural deformation and sustainability.

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- (21) International Application Number:
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- (22) International Filing Date:
09 November 2021 (09.11.2021)
- (25) Filing Language:
English
- (26) Publication Language:
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- (71) Applicant: **FLEXCRETE TECHNOLOGY LIMITED**
[CN/CN]; Unit 6, 15/F., Tower 1, Ever Gain Plaza, 88 Container Port Road, Kwai Chung, New Territories, Hong Kong (CN).
- (74) Agent: **RUNPING & PARTNERS**; Suite 515, Yingu Mansion, No.9 Beishuansilu, Haidian District, Beijing 100190 (CN).
- (81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DJ, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, IT, JO, JP, KE, KG, KH, KN, KP, KR, KW, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, WS, ZA, ZM, ZW.
- Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).
- Published:
— with international search report (Art. 21(3))
— with amended claims and statement (Art. 19(1))

(54) Title: ELASTIC REINFORCED COMPOSITE FOR FORMING DIVERSE STRUCTURAL SYSTEMS AND ITS APPLICATION IN MONOLITHIC SANDWICH MATERIAL COMPOSITE

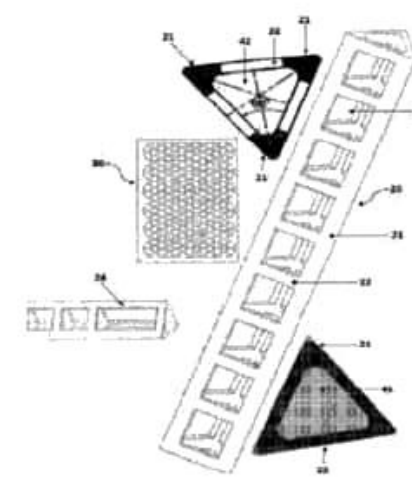


FIG. 4

(57) Abstract: Fabrication and design of novel reinforced cementitious composite (10) made up of seamless elongate monolithic perforated tubular metallic reinforcement bar (20) with triangular sectional confinement topology configured by three continuous parallel aligned interconnected solid rod-like portion located at triangular apices respectively as longitudinal reinforcing phase (21), multiple perforated mid-span shell bandage as anchorage phase (22), and infiltrated heterogeneous blend tunable low hydration heat high elastic modulus hydraulic binder material as matrix phase (40) characterized by a unique, core-radial, axial-align, distributed mechanical bond anchorage dowel network (41) effected from multi-cellular matrix dowel unit cells (42) synergistically formed unitarily with endless cellular confinement hoops along the perforated mid-span shell during hydraulic binder composite solidification and its use therewith multi-layer perforated metallic plates as transversal reinforcing phase (30) for fabricating diverse three-dimensional reinforcement bar network confinement cage in constructing reinforced solid concrete elements of buildings and civil structures.

WO 2023/082040 A1

[Continued on next page]

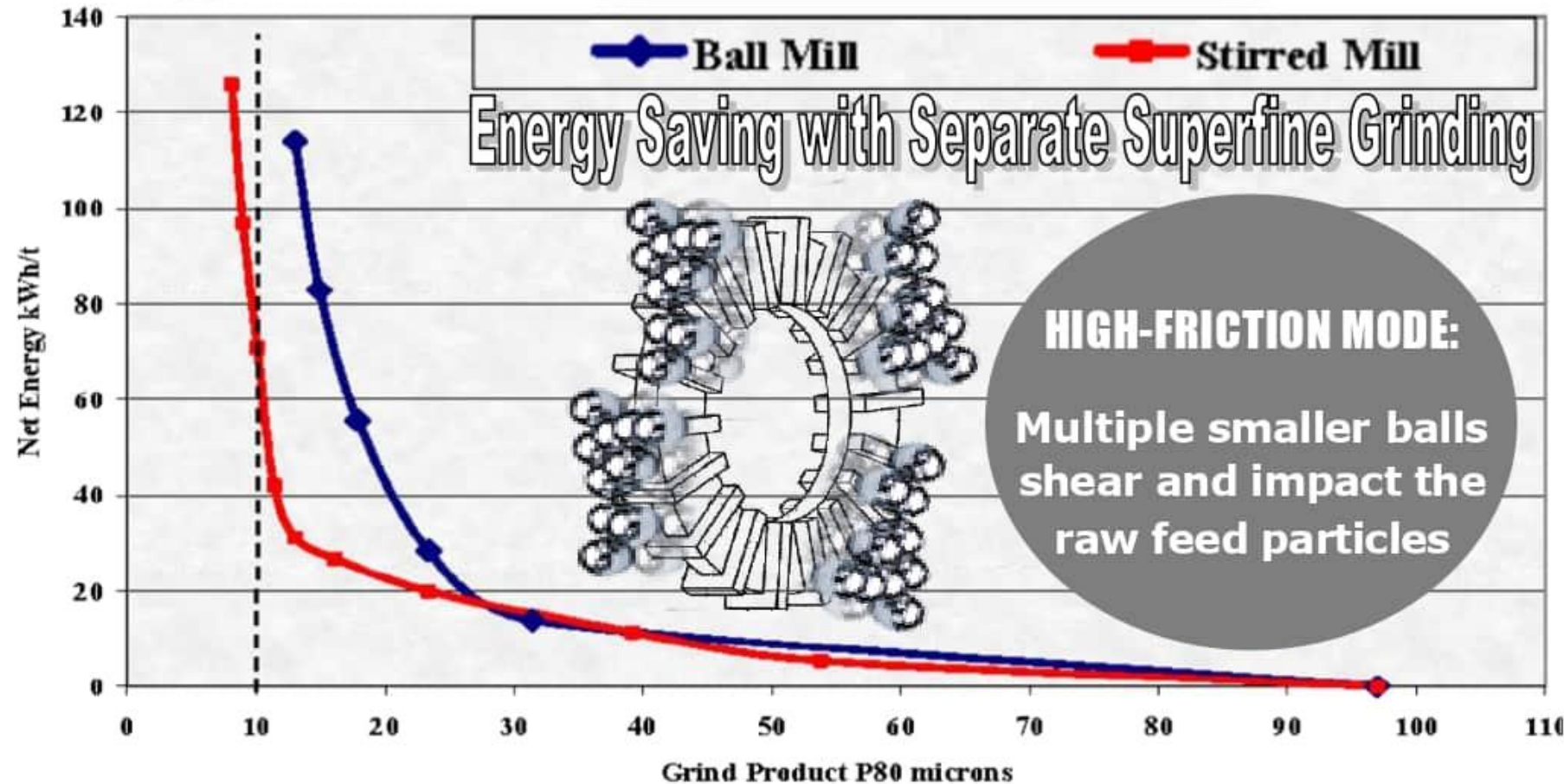
MAR MILL

G.Seed
Superfine GGBS



Our Innovative Grinding Approach

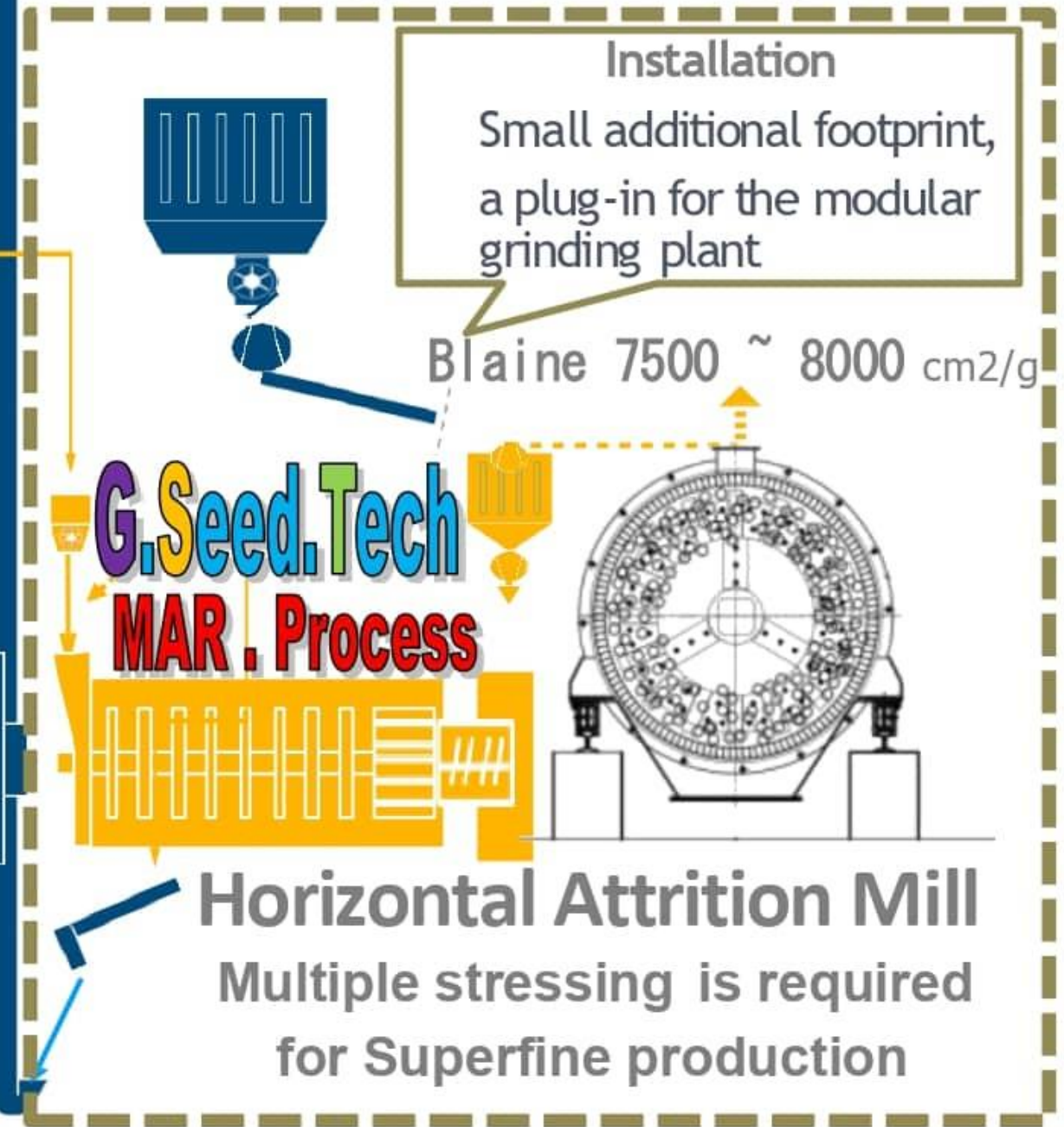
Eligible SCM MANUFACTURING



Raw Slag Slag Primary Coarse Grinding Circuit



G.Seed Superfine GGBS Plug-in Grinding Circuit



Efficient grinding process for coarse to medium grain size by compression

Novel Agitator

Horizontal Dry Grinding

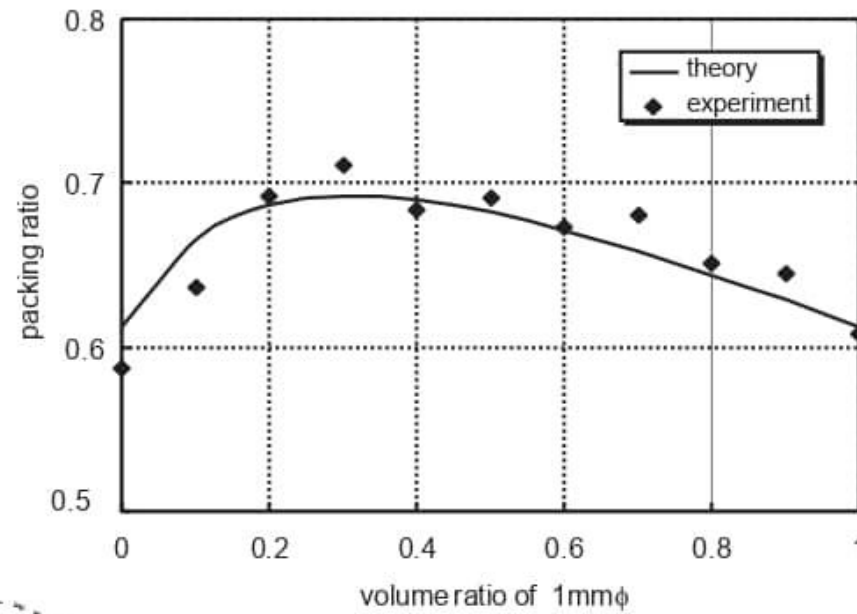
Non-Classifer

Continuous Mode 03-3

Core-Shell Microstructure – Local Dense Packing



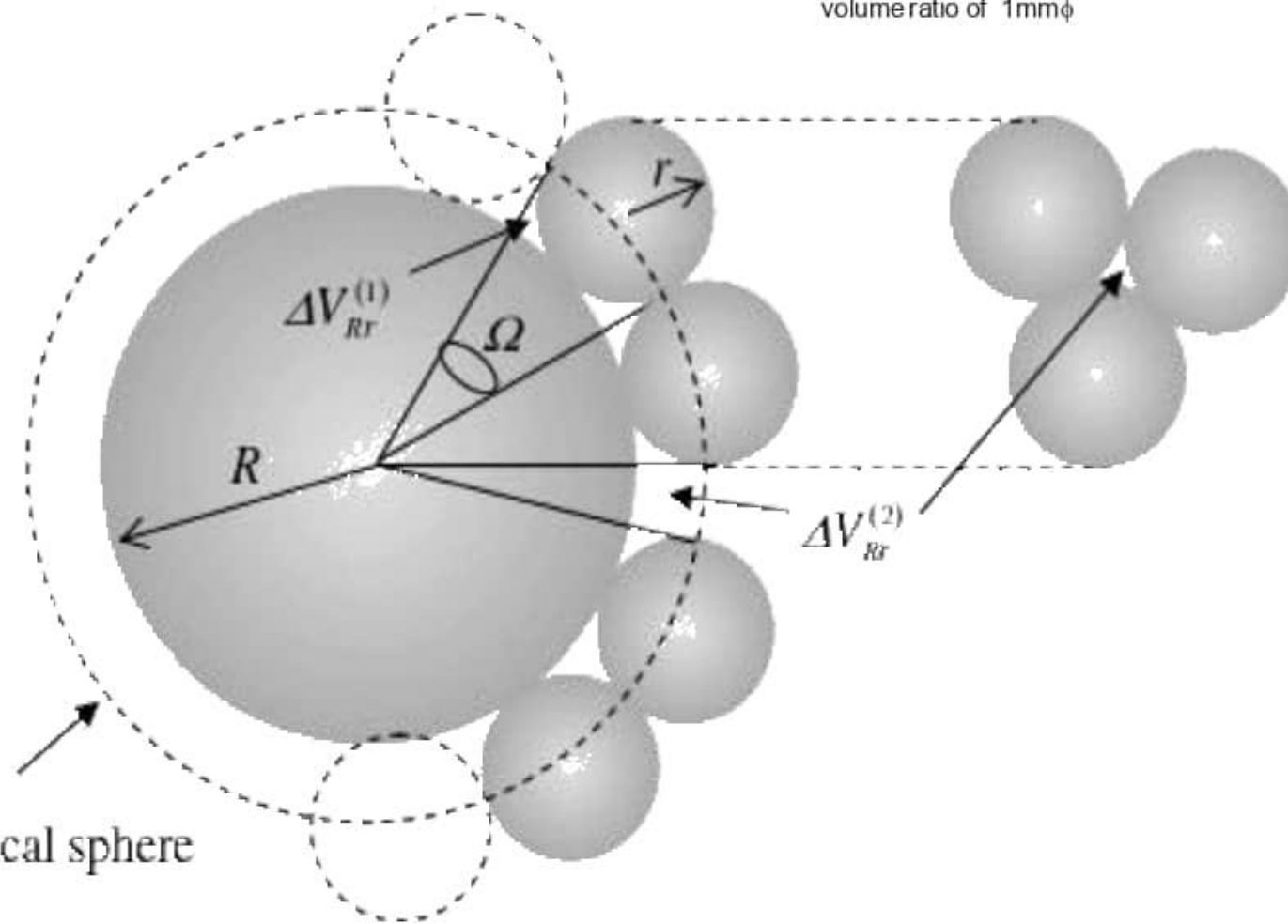
Simple system consisting of single type of particles (5mm ϕ)



Packing density of mixed-particle system comprising particles with two different radii. The horizontal axis represents the volume ratio of particle diameter of 1 mm.



System with particles having two different diameters particles (1mm ϕ : 5mm ϕ = 3 : 7)



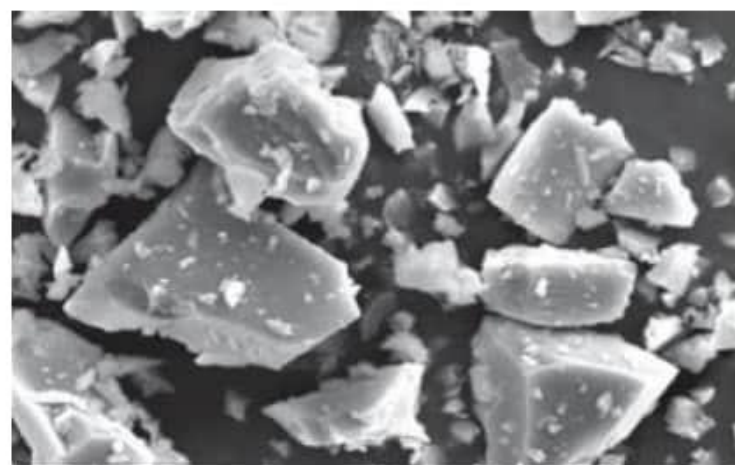
Hypothetical sphere

Packing of spheres with radius r in direct contact with sphere with radius R .

Japan GGBS Slag Activity Index And Blaine Fineness

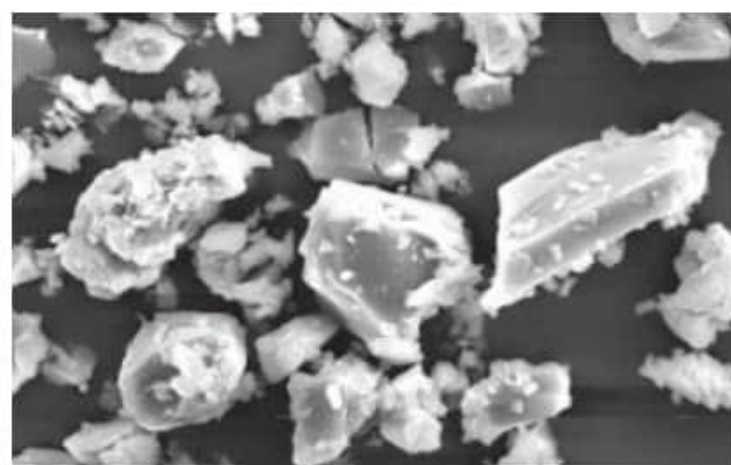
各種高炉スラグ微粉末の SEM 画像

BF4000



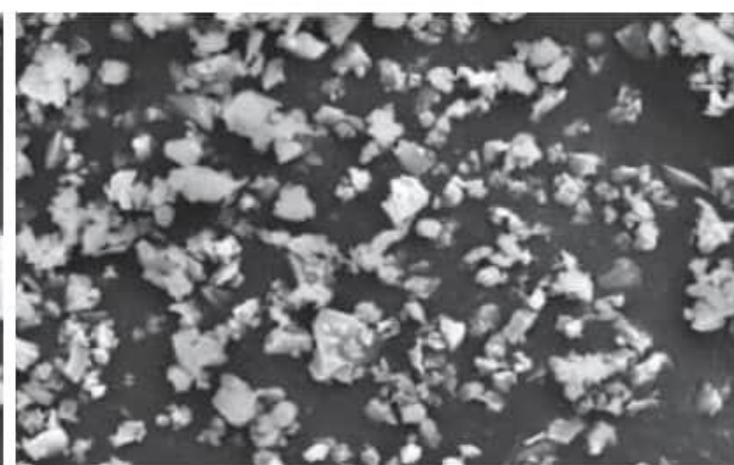
1000倍 5μm

BF8000



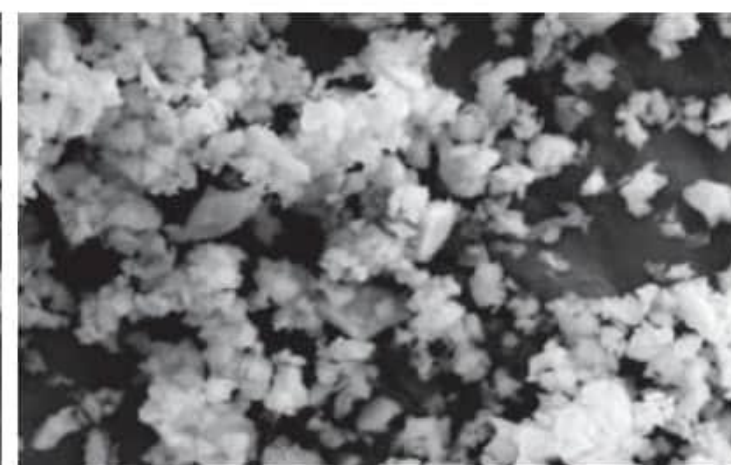
1000倍 5μm

BF11000



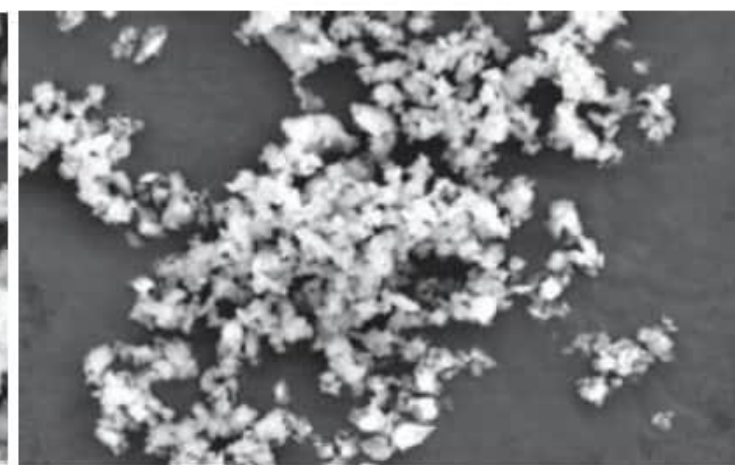
1000倍 5μm

BF18000



1000倍 5μm

BF30000

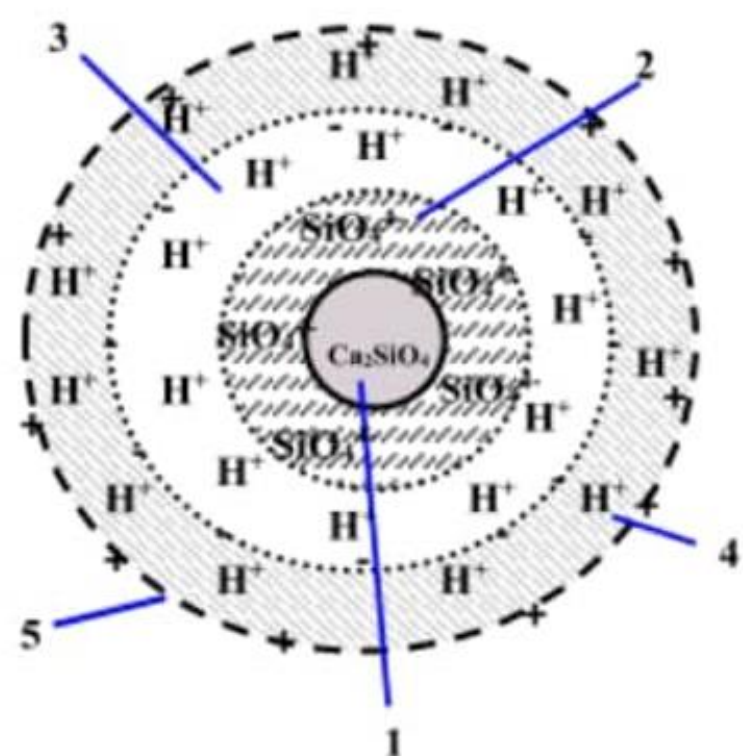


1000倍 5μm

- BF4000
- BF11000
- BF30000
- - - - BF8000
- BF18000

高炉スラグ微粉末の種類および物性

Production Using Air Classifier	種類				
	BF4000	BF8000	BF11000	BF18000	BF30000
密度(g/cm ³)	2.92	2.92	2.92	2.92	2.92
比表面積(cm ² /g)	4830	8180	10800	18050	29620
平均粒径(μm)	9.6	5.2	4.0	2.0	1.0
フロー値比(%)	100	99	98	93	86
活性度 指数 (%)	7日	67	98	100	154
	28日	99	112	128	138
	91日	105	120	122	118

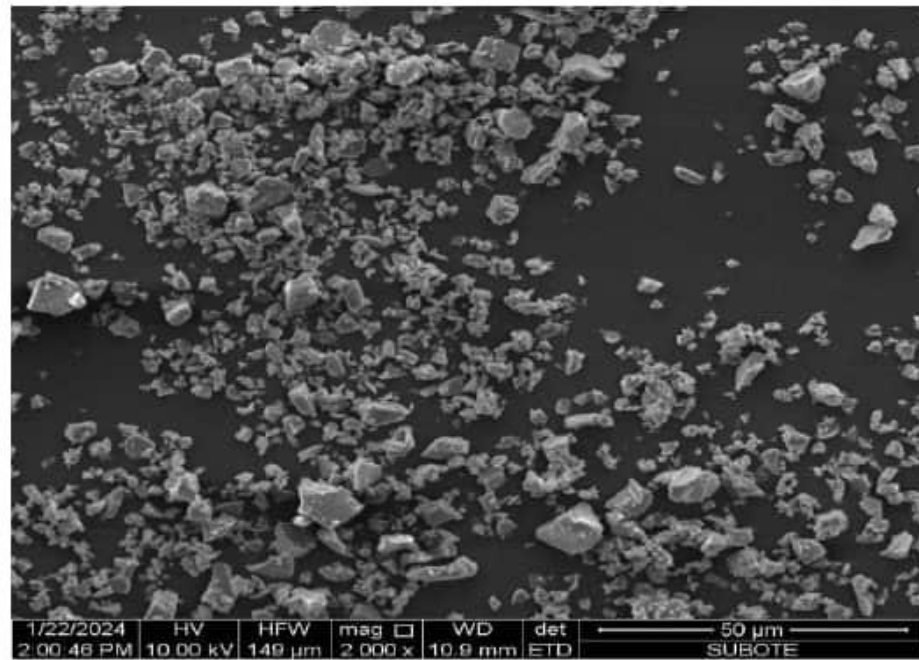


高炉スラグ微粉末の
化学成分

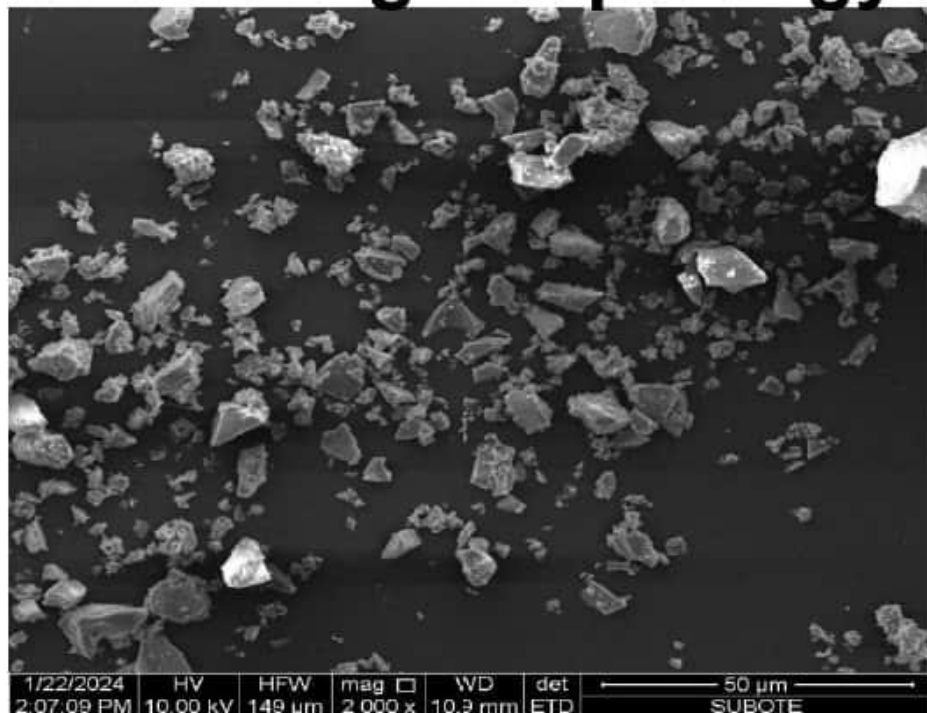
化学成分 (%)	試験値	JIS A 6206 の規定値
ig.loss	0.55	3.0 以下
insol	0.64	—
SiO ₂	32.7	—
Al ₂ O ₃	13.4	—
Fe ₂ O ₃	0.5	—
CaO	41.6	—
Na ₂ O	0.22	—
K ₂ O	0.28	—
MgO	6.9	10 以下
SO ₃	0.34	4.0 以下
Cl ⁻	0.0003	0.02 以下

High Fineness GGBS Particle Shape

Superfine GGBS Slag



Rounding Morphology



S95 GGBS Slag

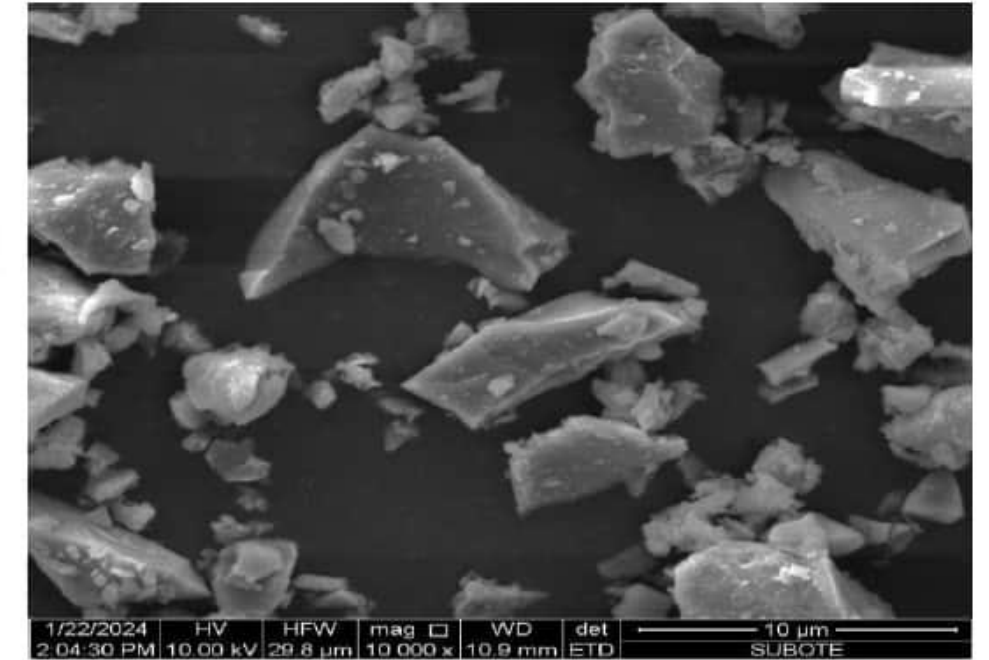
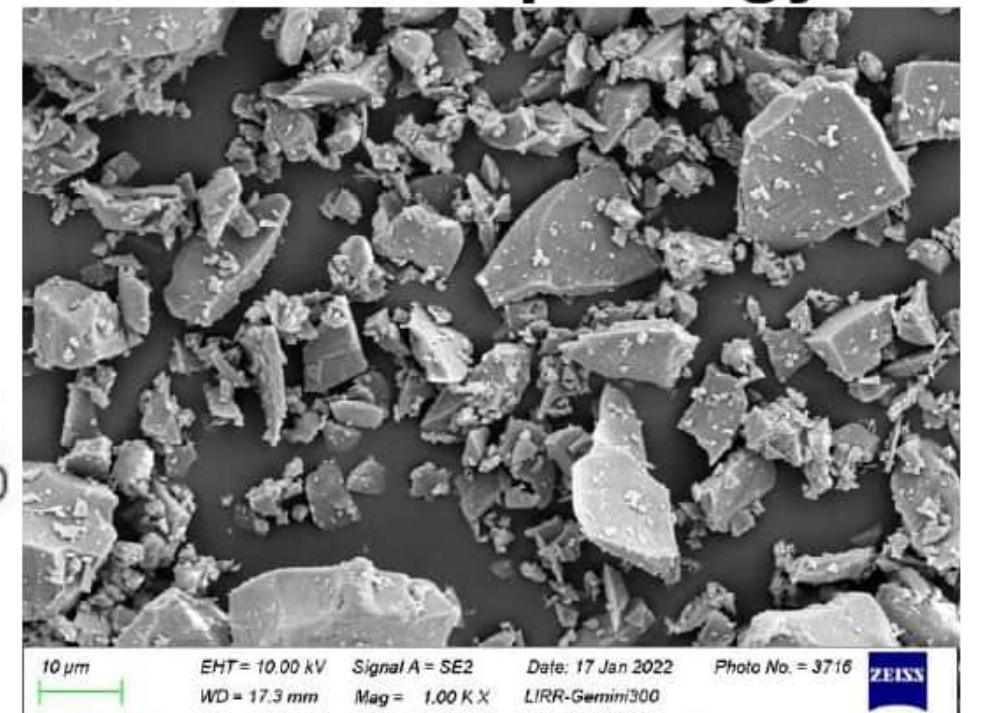
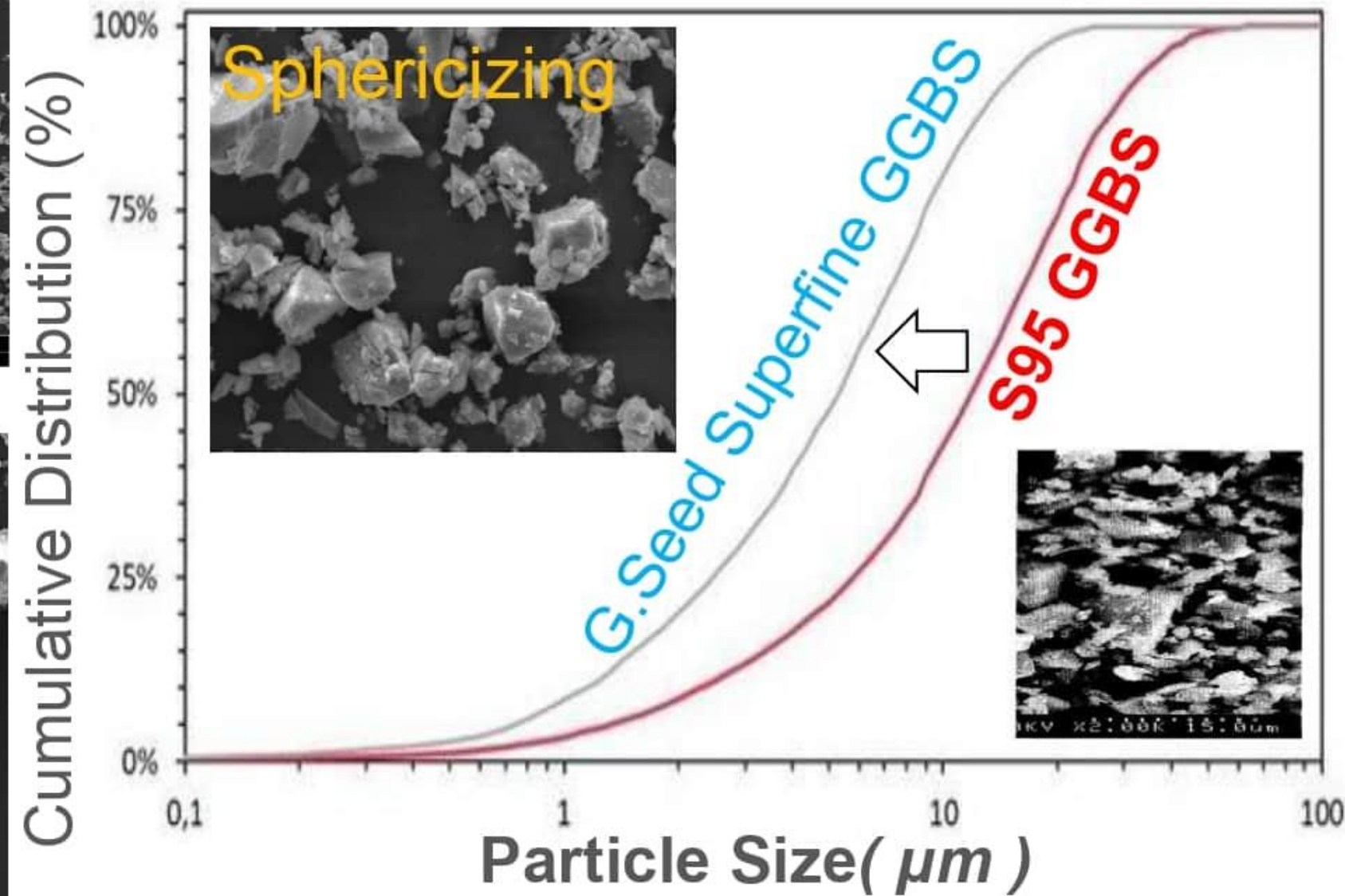


Plate Morphology



MAR . Process



Superfine GGBS Fineness and Substitution Rate On Concrete Properties

	Type	S 95 GGBS 4000			Ground granulated blast-furnace slag 6000			<i>G.Seed Superfine GGBS</i> 8000		
		3000	≅	< 5000	5000	≅	< 7000	7000	≅	< 10000
		35	50	70	35	50	70	35	50	70
Property of fresh concrete	Fluidity	○	○	○	◎	◎	◎	◎	◎	○
	Bleeding	○	○	△	◎	◎	◎	◎	◎	◎
	Setting delay effect	◎	◎	◎	◎	◎	◎	◎	◎	◎
	Adiabatic temperature rise	–	–	◎	–	–	◎	–	–	◎
	Heat generation rate restraint	○	◎	◎	○	○	◎	○	○	◎
Property of strength	Initial strength	○	△	△	○	○	△	○	○	◎
	28 days strength	○	○	△	○	◎	◎	◎	◎	◎
	Long-term strength	○	◎	◎	○	◎	◎	◎	◎	◎
	High strength	○	△	△	○	◎	◎	◎	◎	◎
Property of durability	Drying shrinkage	○	○	○	○	○	○	○	○	○
	Carbonation	–	–	△	–	–	△	–	–	△
	Freeze thaw	○	○	○	○	○	○	○	○	○
	Water-tightness	○	◎	◎	○	◎	◎	○	◎	◎
	Salt shield	○	◎	◎	○	◎	◎	○	◎	◎
	Seawater resistant	○	◎	◎	○	◎	◎	○	◎	◎
	Acid and sulfates resistant	○	◎	◎	○	◎	◎	○	◎	◎
	Heat resistant	○	○	○	○	○	○	○	○	○
	Alkali-silica restraint	○	◎	◎	○	◎	◎	○	◎	◎
Abrasion resistance	○	○	○	○	○	◎	○	◎	◎	

Legend:

◎ : Good property is provided in comparison with no mixture concrete.
○ : At the same level or a little good property is provided.

△ : Attention is necessary for use.
– : Property varies according to a condition.

G.Seed Concrete

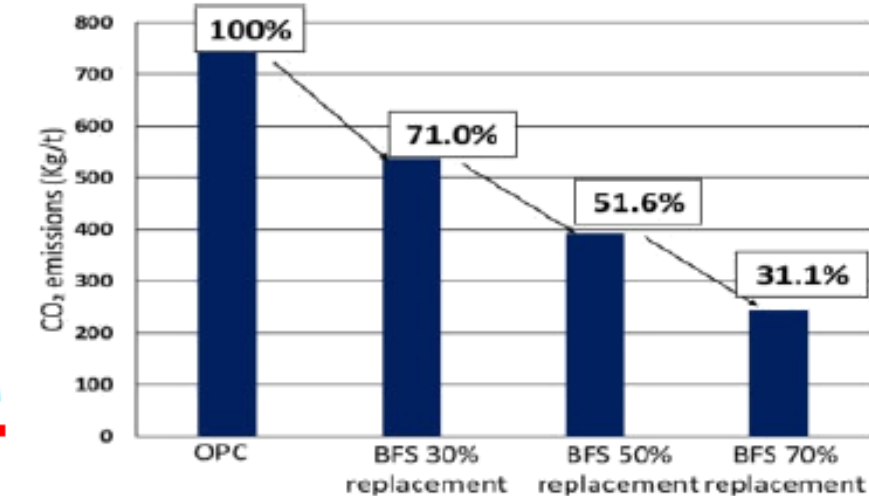
Binder Content	Compressive Strength (Mpa)	Elastic Modulus (GPa)	
450Kg-540Kg	Grade C60-C90 _(Cylinder)	40-45	/ 46-50
Aggregate Type :		Granite Aggregate Granite Stone Fines	Basalt Aggregate River Sand/Stone Fines
Water/Binder Ratio : 0.27 – 0.32		Workability : Flow Table Value 550 – 650 mm	

Paste Performance



Elastic Modulus + Flexural Toughness + Compressive Strength
↑ ↑ ↑
Gel Morphology Defect Length Volume Porosity

- Low Capital Carbon Approach
- Increased Service Life and Durability
- Reduce Steel Reinforcing And Structural Member Size
- And Most Importantly=> **Carbon Reduction & Cost Saving



CONCRETE STRENGTH AND MODULUS OF ELASTICITY engineer design value

Code of Practice for
Structural Use of Concrete
2013 Design values of elastic modulus for normal-weight concrete

Concrete Strength Grade	E_c (kN/mm ²)	
	For general use	For checking overall building deflection (see note 2)
C20	18.7	20.5
C25	20.5	22.2
C30	22.2	23.7
C35	23.7	25.1
C40	25.1	26.4
C45	26.4	27.7
C50	27.7	28.9
C55	28.9	30.0
C60	30.0	31.1
C65	31.1	32.2
C70	32.2	33.2
C75	33.2	34.2
C80	34.2	35.1
C85	35.1	36.0
C90	36.0	36.9
C95	36.9	37.8
C100	37.8	38.7

HPC & UHPC Concrete E-Value : China Code

超高强混凝土的强度和弹性模量 (MPa)						
混凝土强度等级 $f_{cu,k}$		C70	C80	C90	C100	C110
标准值	轴心抗压 f_{ck}	45.0	51.0	56.0	61.0	67.0
	轴心抗拉 f_{tk}	3.0	3.1	3.3	3.5	3.8
设计值	轴心抗压 f_{cd}	31.8	36.1	40.0	43.7	48.0
	轴心抗拉 f_{td}	2.1	2.2	2.4	2.5	2.7
弹性模量 E_c ($\times 10^4$)		3.7	3.7	3.8	3.9	4.0
UHPC 立方体抗压强度标准值 U_{cuk} 不应小于 120MPa						
强度等级	UC 120	UC 140	UC 160	UC 180	UC 200	
u_{cuk} (MPa)	120	140	160	180	200	
f_{Uck} (MPa)	84	98	112	126	140	
f_{Ucd} (MPa)	58	68	77	87	97	
UHPC 弹性模量 E_c ($\times 10^4$)						
强度等级	UC 120	UC 140	UC 160	UC 180	UC 200	
弹性模量	4.2	4.5	4.8	5.1	5.4	

Green Active Robustness Concrete

Binder 420 - 520Kg (50% G.Seed)

E.Modulus - Product Trial Data

Done By FLEXCRETE

Design Of 1m ³ Concrete														Compressive Strength (MPa)				Elastic Modulus
Batch	Mix Volume	Cement (KG)	Flexcrete-UFGBBS (KG)	S/F (KG)	Aggregates (5-10mm) (KG)	River Sand (KG)	Z-Additives (KG)	A-Catalyst (KG)	Water (KG)	SBT RW-BP (L)	HEMI (L)	PCA-1 (L)	Remarks	12-Hour	24-Hour	7-Day	28-Day	
4th	0.04	210	210	980	770	0	0	0	134.4	1	2	7.5	Cement Reduction	Nil	18 MPa	91 MPa	99 MPa	48.5 Gpa
5th	0.04	260	234	880	770	0	26	0	166.4	1	2	6	Zeolites	Nil	28 MPa	74 MPa	79 MPa	47.0 Gpa
6th	0.04	260	260	880	770	0	0	0	166.4	1	2	6		1.5 MPa	18 MPa	88 MPa	96 MPa	46.8GPa



Customer Sample No.	Batch 4-1G
HKT Sample No.	P24C00165
Date Cast	6 Feb 2024
Age at test (days)	28
Condition of cylinder when received	Dry
Curing and storage report	Curing in laboratory at 27+/-3°C
Type of measuring instrument	Dial Gauge
Gauge length (mm)	150.9
Diameter of cylinder (mm)	150.0
As Received density * (kg/m ³)	2400
Concrete cube strength (MPa)	102.2
Maximum applied stress (MPa)	27.2
Compressive strength of cylinder (MPa)	93.34
Static modulus of elasticity (MPa)	
Static modulus of elasticity (GPa)	

Customer Sample No.	Batch 5-1G
HKT Sample No.	P24C00167
Date Cast	6 Feb 2024
Age at test (days)	28
Condition of cylinder when received	Dry
Curing and storage report	Curing in laboratory at 27+/-3°C
Type of measuring instrument	Dial Gauge
Gauge length (mm)	150.9
Diameter of cylinder (mm)	150.0
As Received density * (kg/m ³)	2400
Concrete cube strength (MPa)	80.6
Maximum applied stress (MPa)	20.98
Compressive strength of cylinder (MPa)	76.77
Static modulus of elasticity (MPa)	43,500
Static modulus of elasticity (GPa)	47.0

Customer Sample No.	Batch 6-1J
HKT Sample No.	P24C00170
Date Cast	6 Feb 2024
Age at test (days)	28
Condition of cylinder when received	Dry
Curing and storage report	Curing in laboratory at 27+/-3°C
Type of measuring instrument	Dial Gauge
Gauge length (mm)	150.8
Diameter of cylinder (mm)	150.0
As Received density * (kg/m ³)	2400
Concrete cube strength (MPa)	93.4
Maximum applied stress (MPa)	24.9
Compressive strength of cylinder (MPa)	97.96
Static modulus of elasticity (MPa)	46,800
Static modulus of elasticity (GPa)	46.8

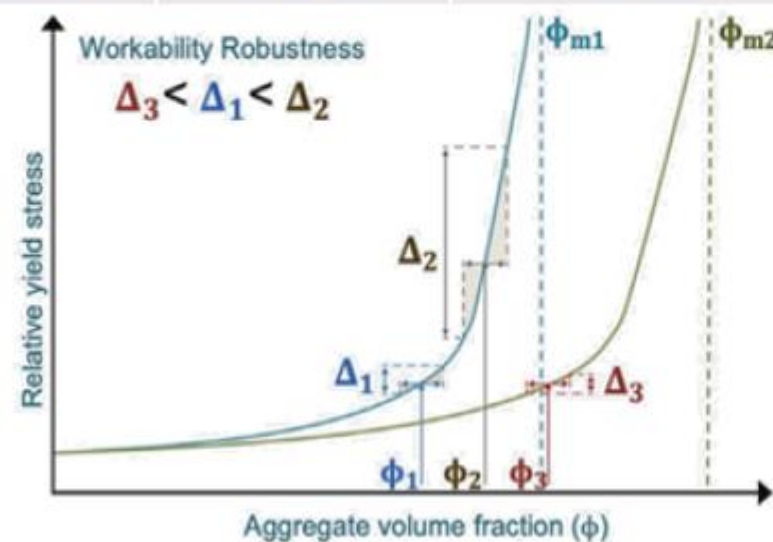
Test Done By Nami



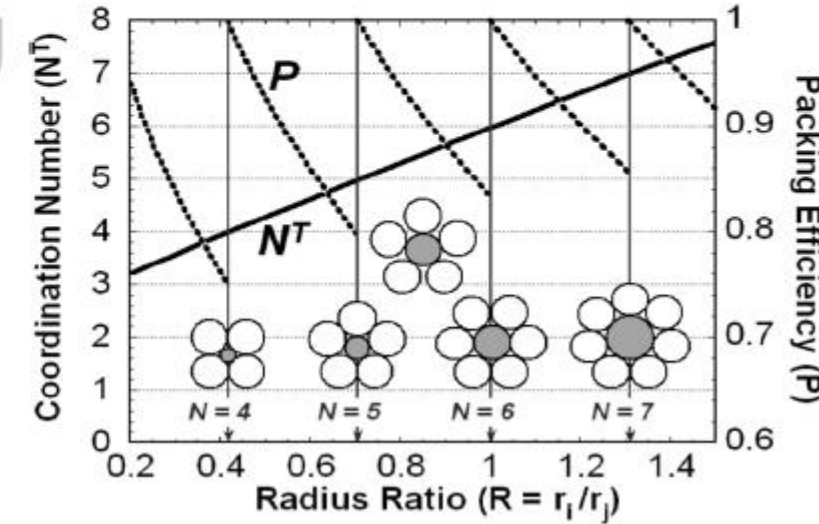
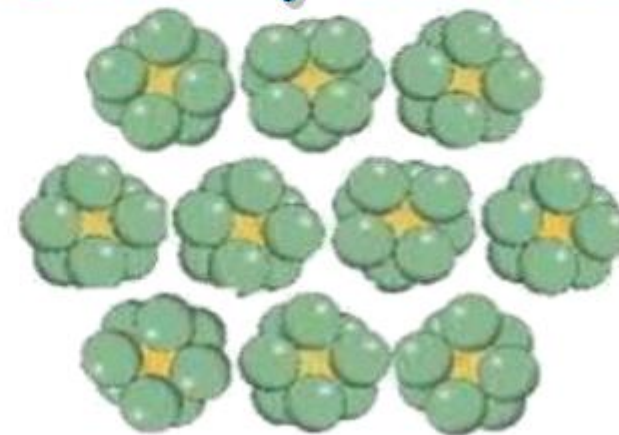
Green Active Robustness Concrete

Binder : 520 KG/M3 (50% G.Seed Superfine GGBS)
 (Fine Aggregate : Granite Stone Fines) (Coarse Aggregate : Granite-10mm & 20mm)

No.	w/b	S/A	Paste volume	Bulk Density	Flow table value	Compressive Strength	Elastic Modulus
				Kg/m3	mm	MPa	GPa
Batch 4-2	0.307	0.53	0.35	2370	300	<u>55.7</u>	<u>42.5</u>
M10-0.34	0.320	0.50	0.34	2400	400	<u>66.1</u>	<u>42.2</u>
M10-0.34-1	0.306	0.50	0.34	2400	550	<u>99.0(56d)</u>	<u>45.8</u>
M10-0.34-2	0.306	0.50	0.34	2405	530	<u>98.0</u>	<u>44.8</u>



Local Packing - Global Packing



High Grade – No Silica Fume Mix

14 Days Test Result

Plastic Density (Kg/M ³)	2390	
Yield	0.999	
Initial (Slump Slump Flow)	225	
Cube Age (Day)	Strength	Test Date
3	84.5, 84.7	18/03/2024
7	103.2, 105.6	22/03/2024
28		12/04/2024

Lab Trial No.	LTM5988				
Date Cast	15/03/2024				
Concrete Mix	SOD/20GGBS+CSF				
Slump Flow	200				
Volume (M ³)	Design (1m ³)	Final (1m ³)	0.045	Initial	After Adjust (+/-)
Cement (Kg)	273	273	12.29		
PFA (Kg)	0	0	0.00		
GGBS (Kg)	274	274	12.33		
Silica Fume (Kg)	0	0	0.00		
20mm (Kg)	565	565	25.43	0.03	25.45
10mm (Kg)	435	435	19.58	0.18	19.75
CRF (Kg)	410	410	18.45	0.37	18.82
R.S (Kg)	270	270	12.15	0.30	12.45
Water (Kg)	150	150	6.75	0.87	5.88
RW-BP	1.85	1.85	83ml	RW-BP	
PCA-1	6.56	6.33	285ml	PCA-1	
HEMI	2.50	2.50	113ml	HEMI	
-	0.00	0.00	0ml	-	
-	0.00	0.00	0ml	-	
-	0.00	0.00	0g	-	
-	0.00	0.00	0g	-	
Total Weight (Kg/M ³)	2388	2388			
A/C	3.07	3.07			
W/C	0.27	0.27			

Typical High Strength Concrete Mix

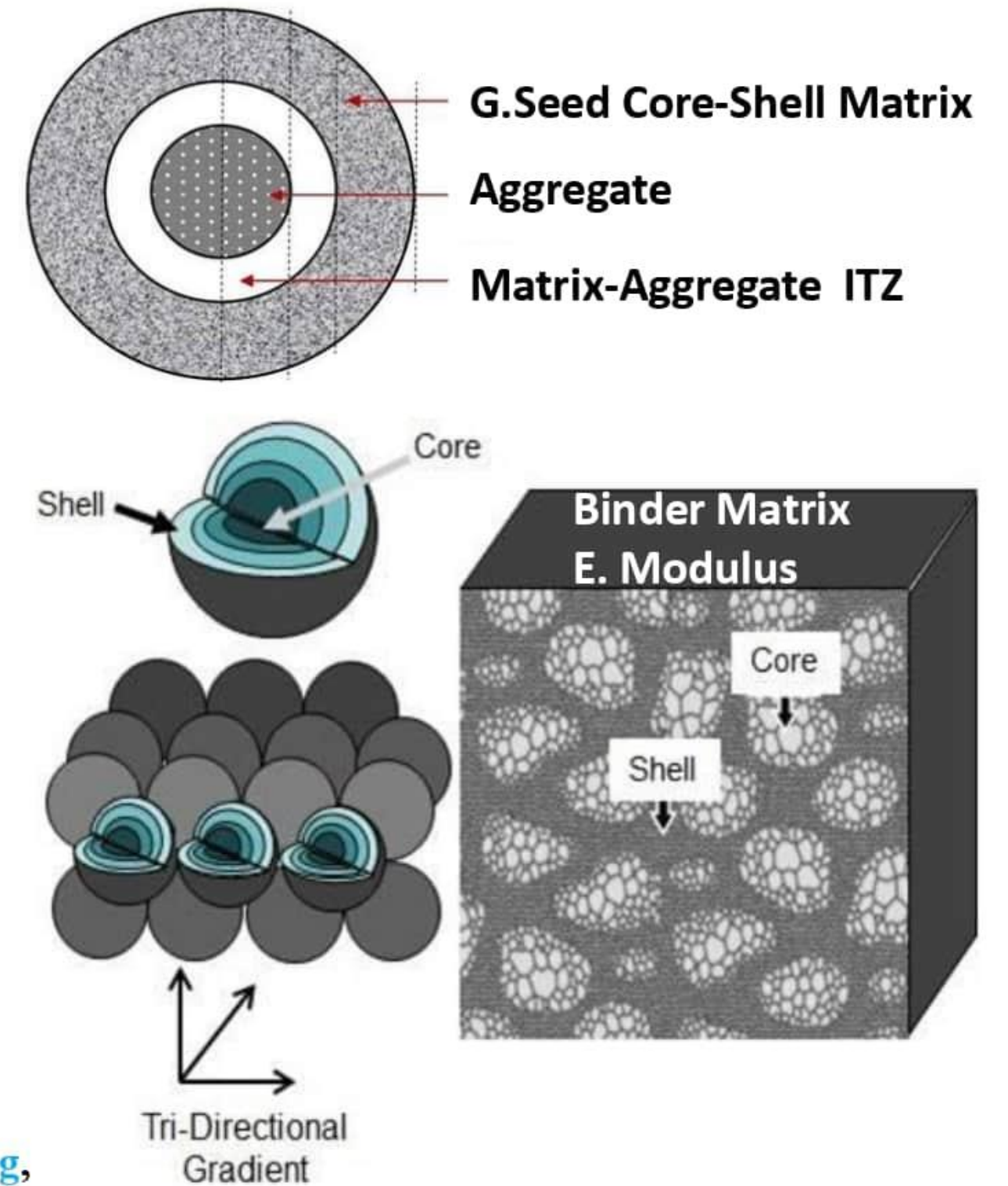
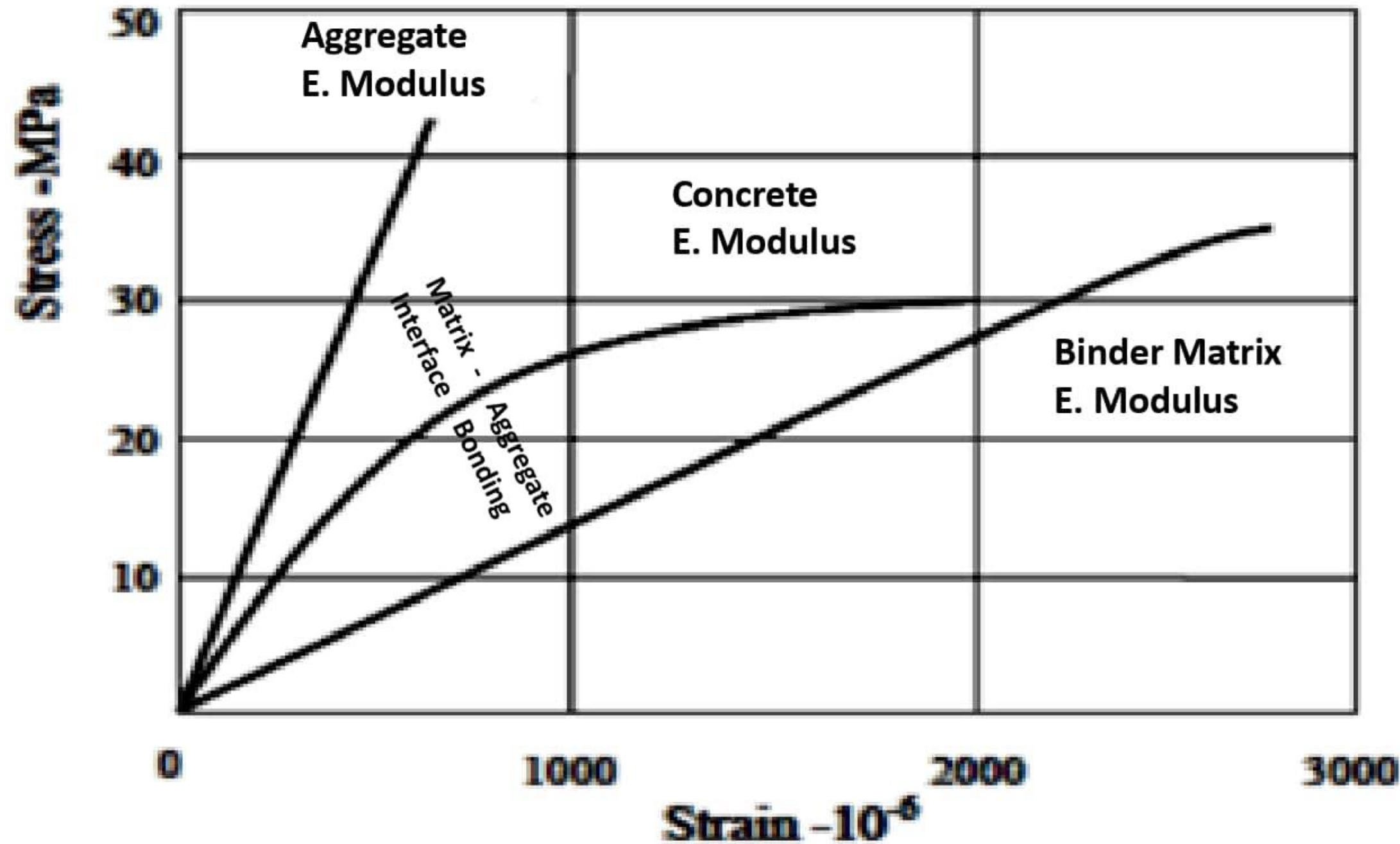
	NAMI's High Strength Concrete		
	C80	C90	C100
Compressive Strength	28 Days		
	98.4MPa	111.8MPa	119.4MPa
Elastic modulus	37.9GPa	39.7GPa	40.7GPa

(b) Determination of Loading	Stress	Loading Force*		
Upper Loading Stress ($\sigma_u = f_c/3$)	36.2 (MPa)	561.2 (kN)		
Basic Stress ($\sigma_b = 0.5MPa$)	0.5 (MPa)	7.8 (kN)		
Cross-sectional area of Cylinder (mm ²)	17694.5			
*Loading force shall be calculated by multiplying the stress by the cross-sectional area of cylinder.				
(b) Determination of Strain Reading	1 st Cycle	2 nd Cycle	3 rd Cycle	Average
Strain under the Upper Loading Stress (ϵ_u)	-311	-314	-312	-312
Strain under the Basic Stress (ϵ_b)	-3.5	-3.8	-3.6	-3.6
The Static Modulus of Elasticity in Compression $[E_c = (\sigma_u - \sigma_b) / (\epsilon_u - \epsilon_b) * 1000, GPa]$	52 GPa 52.0			
Compressive Strength of Test Specimen (MPa)	116 MPa 116			
Compression Testing Machine, Strain Measuring Apparatus, Data Logger (TC-32K)				
Tested By 測試人: _____				
Checked By 查核人: _____ Date of Issue 簽發日期: _____				

(b) Determination of Loading	Stress	Loading Force*		
Upper Loading Stress ($\sigma_u = f_c/3$)	36.2 (MPa)	558.4 (kN)		
Basic Stress ($\sigma_b = 0.5MPa$)	0.5 (MPa)	8.8 (kN)		
Cross-sectional area of Cylinder (mm ²)	12694.5			
*Loading force shall be calculated by multiplying the stress by the cross-sectional area of cylinder.				
(b) Determination of Strain Reading	1 st Cycle	2 nd Cycle	3 rd Cycle	Average
Strain under the Upper Loading Stress (ϵ_u)	-311	-314	-312	-312
Strain under the Basic Stress (ϵ_b)	-3.5	-3.8	-3.6	-3.6
The Static Modulus of Elasticity in Compression $[E_c = (\sigma_u - \sigma_b) / (\epsilon_u - \epsilon_b) * 1000, GPa]$	50.5 GPa 50.5			
Compressive Strength of Test Specimen (MPa)	107 MPa 107			
Compression Testing Machine, Strain Measuring Apparatus, Data Logger (TC-32K)				
Tested By 測試人: _____				
Checked By 查核人: _____ Date of Issue 簽發日期: _____				

Tailoring Concrete Modulus Of Elasticity

The moduli of most materials depend on two factors: bond stiffness, and the density of bonds per unit volume.



Diamond has a very high modulus because the carbon atom is small (giving a high bond density) and its atoms are linked by very strong springs ($S \frac{1}{4} 200 \text{ N/m}$).

Metals have high moduli because close-packing gives a high bond density and the bonds are strong, though not as strong as those of diamond.

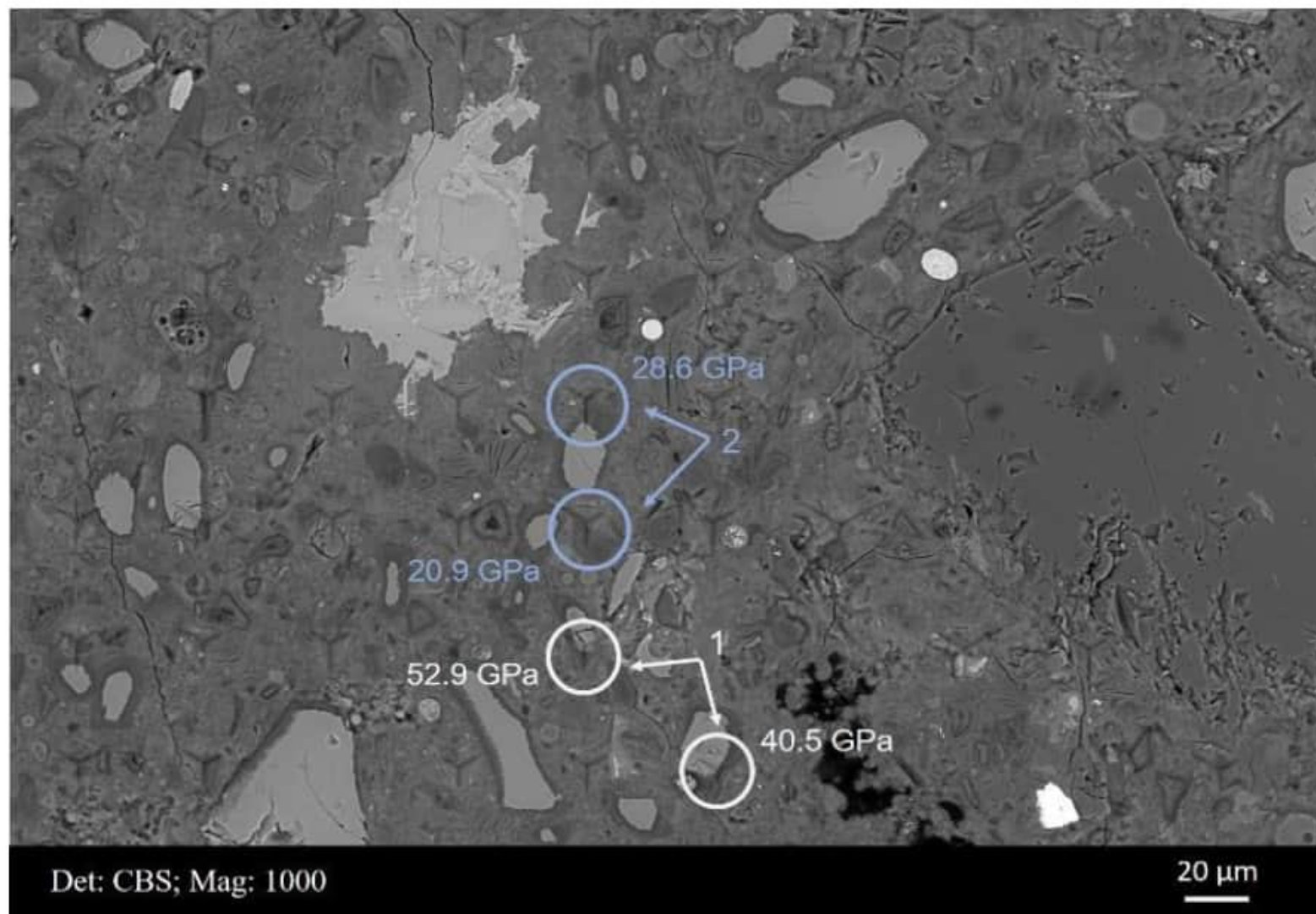
GGBS Grain Size And Hydration Characteristics

Reference

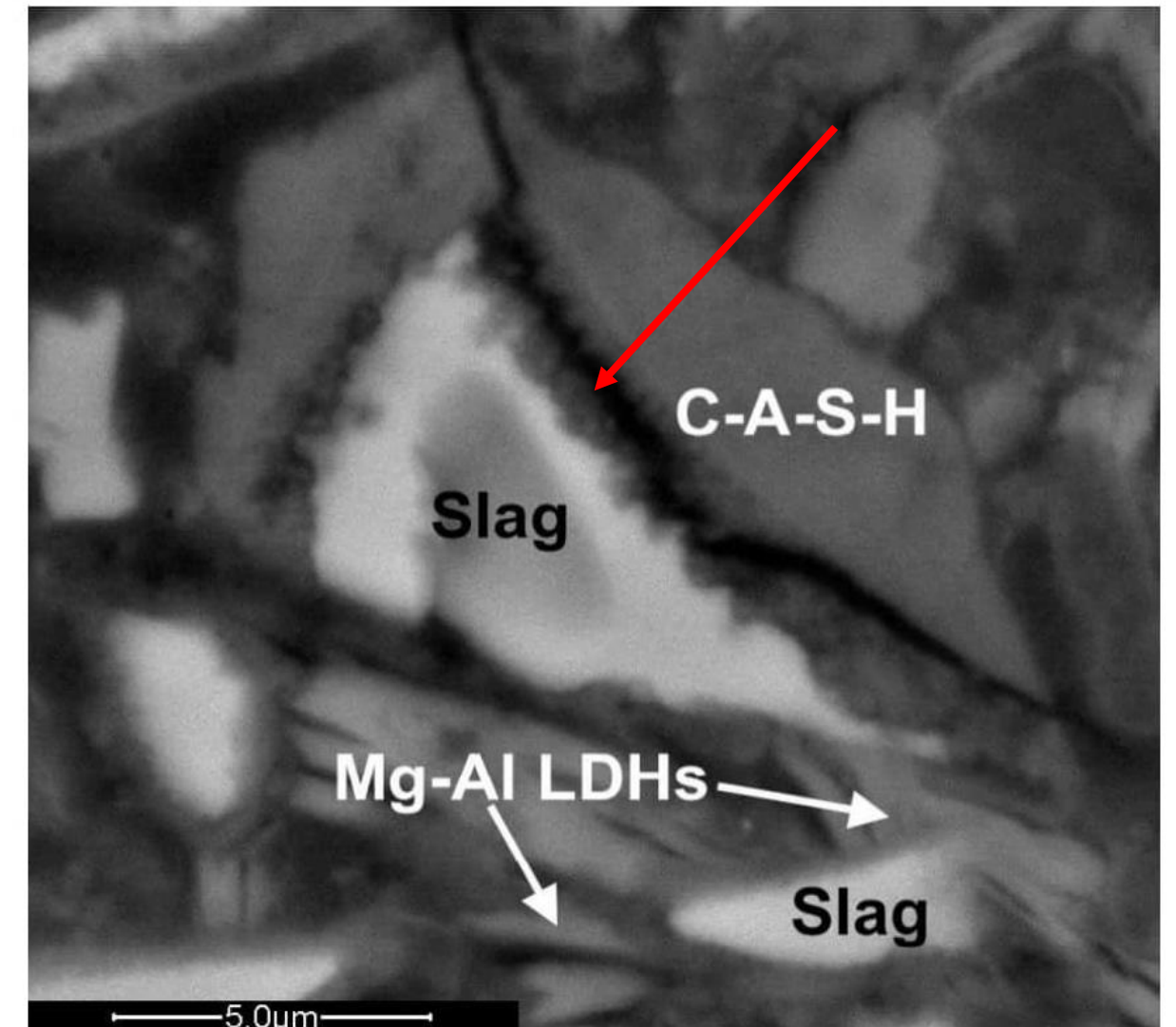
MicroMechanical Properties of Slag Rim Formed in Cement-Slag System

Slag rim mainly consists of secondary precipitations such as C-S-H gel phase and hydrotalcite- like phase, which originate from the hydration of slag.

It was found that, compared to the C-S-H gel phase, slag rim showed about a 15 GPa higher modulus of elasticity.

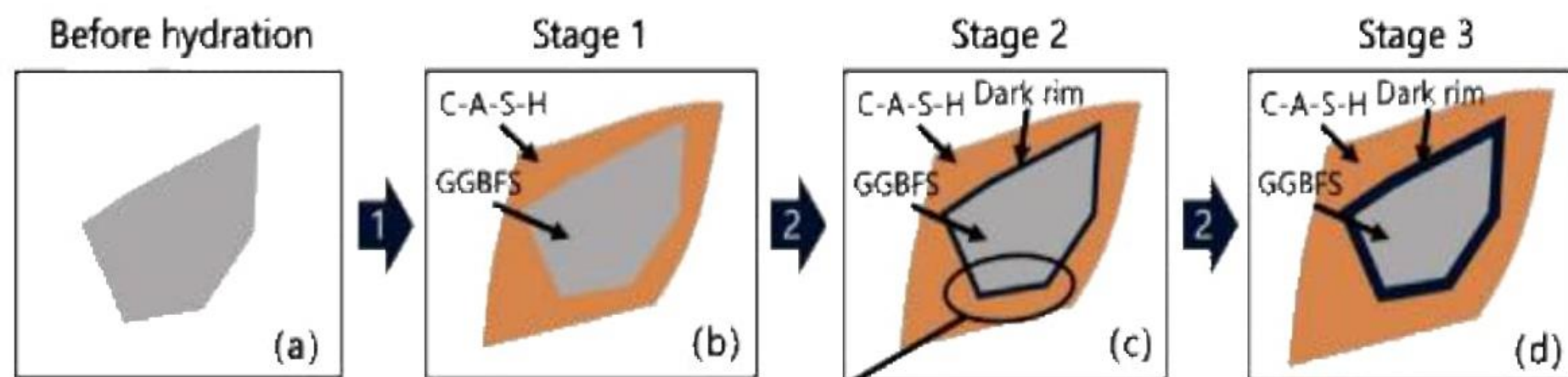


The hydrotalcite-like phase, as the main precipitation of pozzolanic reaction between slag and portlandite, is closely intermixed with the C-S-H gel phase, forming the so-called 'inner' products of slag within the original slag region. The rims around unreacted slag particles, become thicker, and totally hydrated slag grains at a size of >10 μm are also frequently observed.

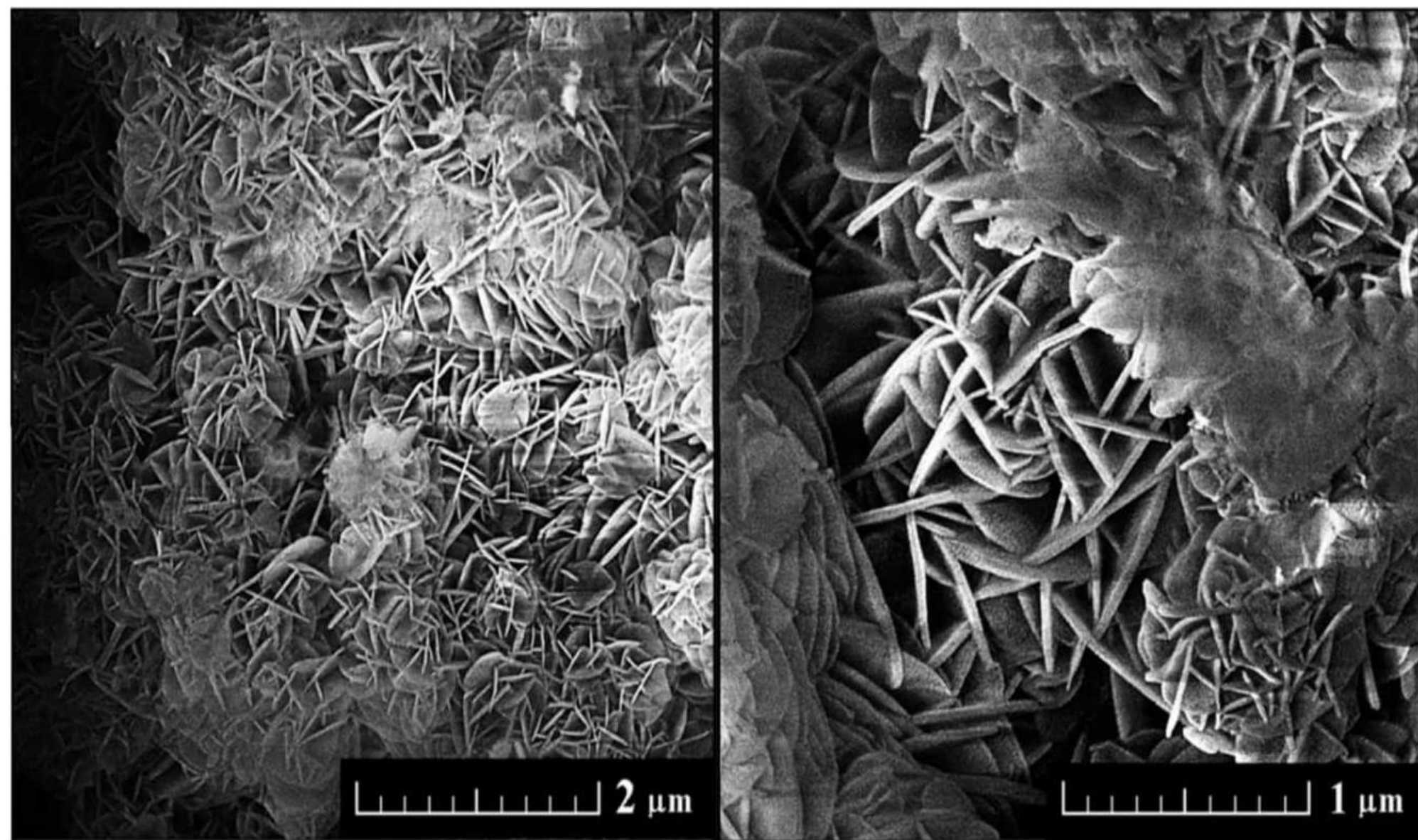
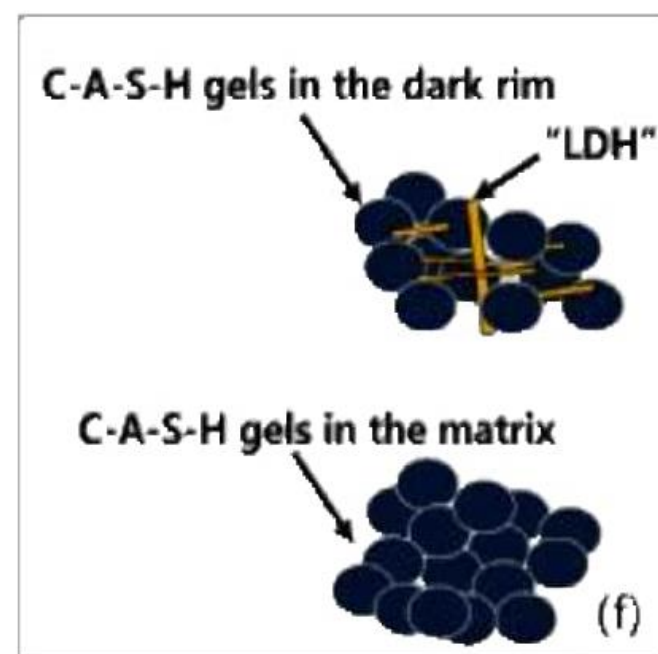
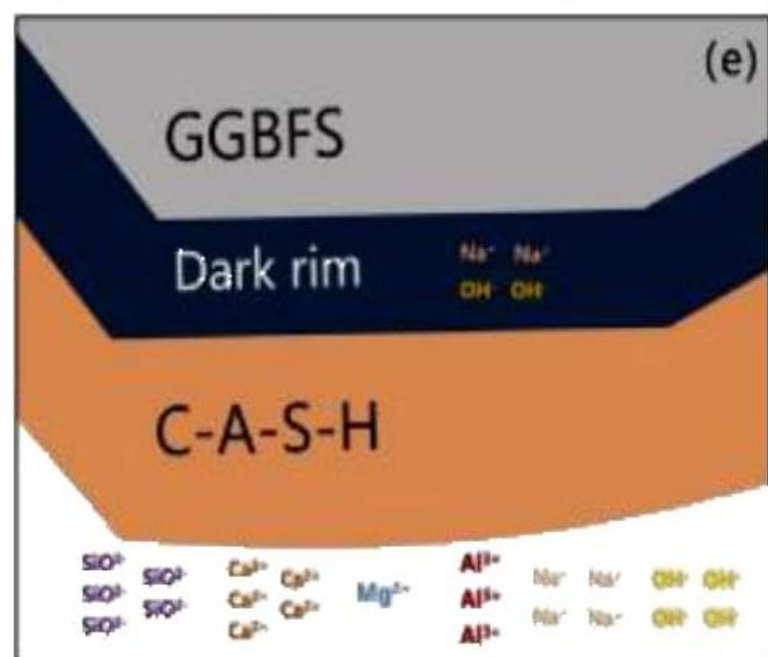


Layered Double Hydroxides - LDH

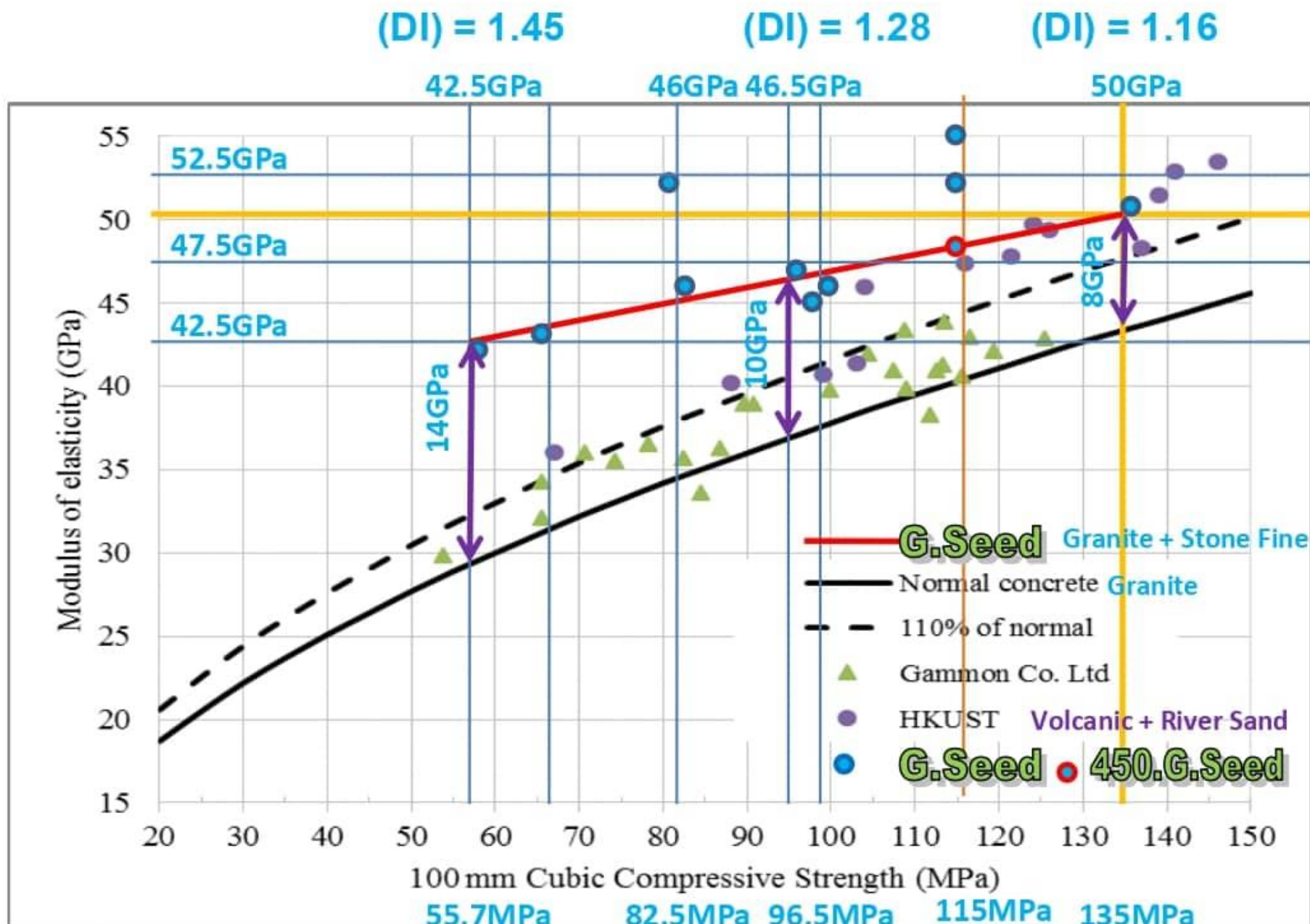
Reference



The dissolution and diffusion of different ions



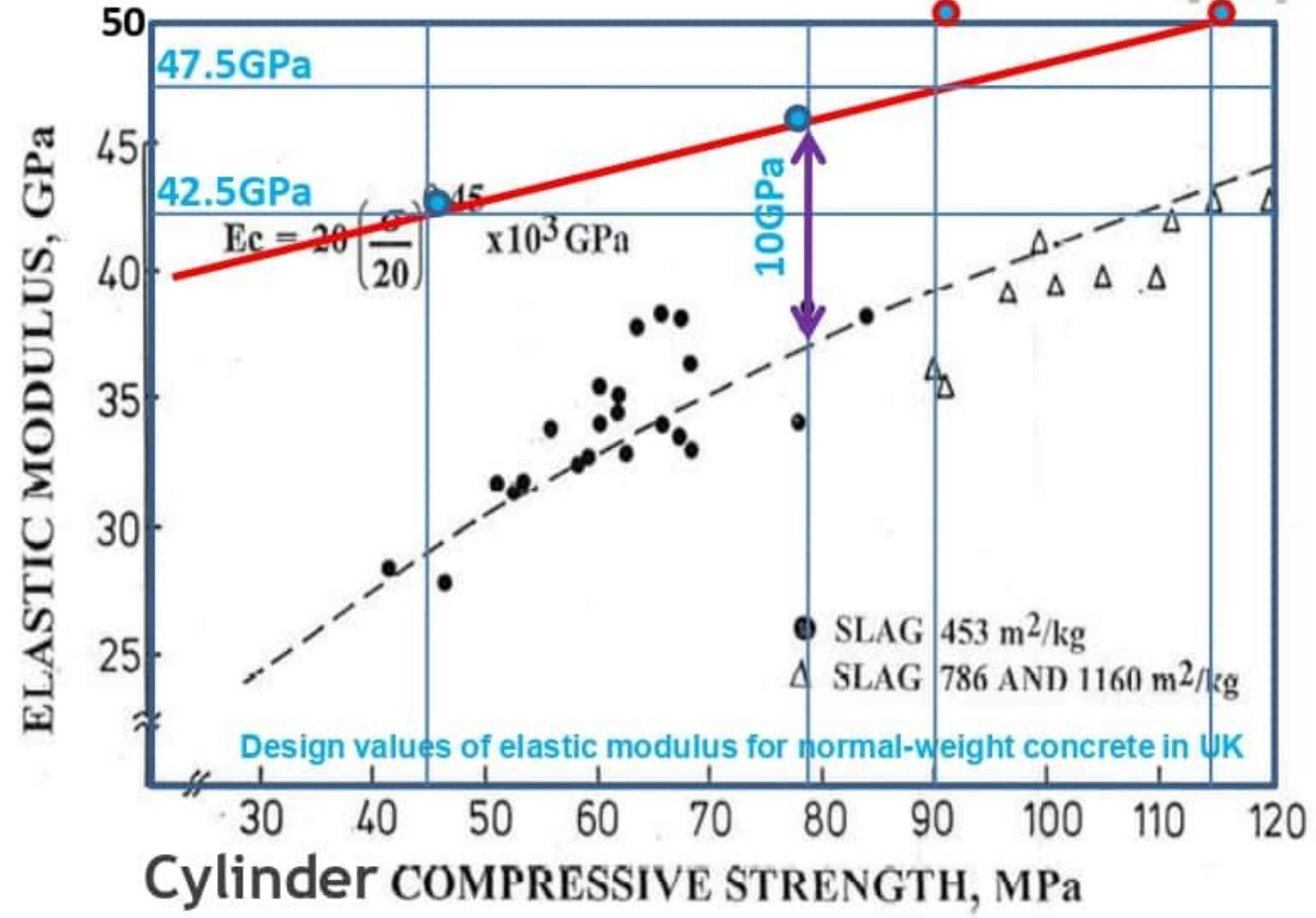
Green Active Robustness Concrete



Design values of elastic modulus for normal-weight concrete in Hong Kong

$E_c = 3.46\sqrt{f_{cu}} + 3.21$ where:
 E_c is the short-term static modulus of elasticity,
 f_{cu} is the cube compressive strength in N/mm^2 .

G.Seed E.Modulus Increment (EI)



450 - Ultra Green Concrete < Grade 80 >

$E_c = 4.45\sqrt{f_{cu}} + 3.13$ where:
 E_c is the short-term static modulus of elasticity,
 f_{cu} is the cube compressive strength in N/mm^2 .
 Deformation Index (DI) = $4.45/3.46 = 1.28$



Thank You